COMPLETE OBSER

CONTAINING THE

Various Methods of finding the LATIT When the SUN is in the MERIDIAN,

By TWO ALTITUDES,

Either Equal or Unequal, when out of the MERIDIAN

A NEW METHOD of finding the LATITUDE

By ONE ALTITUDE ONLY,

AT ANY HOUR WHEN THE SUN CAN BE SEEN,

CORRECTING the WATCH, NEVER BEFORE PUBLISHED.

A NEW METHOD of finding the LATITUDE Without knowing the SUN's DECLINATION,
In any HIGH LATITUDE either NORTH or SOUTH,
And if the DAY of the MONTH be Loft, how to Find it.
With a COMPLETE SET of TABLES.

The METHOD of DETERMINING the

LONGITUDI By LUNAR OBSERVATIONS.

TOGETHER WITH

A New, Concise, Easy, and Infallible Method of DETERMINING the LONGITUDE

By an Observation either of the MOON or Fixt STAR,

BY ONE PERSON ONLY,

And an HADLEY's QUADRANT well adjusted.

By THOMAS HARRISON and SON.

Y O R K: PRINTED IN THE YEAR 1788.

COMPLETE OPSERVATOR

Various Methods of Arting the Late 1 (1) 2 (1)

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PREFACE.

WHEN we confider the utility of observations to mariners in general, and to those that trade into foreign parts in particular, we need not be surprised that so many efforts have been made to bring this useful branch of learning to the utmost degree of perfection: and though a vast extent of tracts on this subject have appeared, yet none have been under our inspection that have handled every circumstance easy to be understood by the generality of readers. In this small treatise we have endeavoured to render every example as easy as possible, and we hope it will enable those who are acquainted with the first principles, to attain (without the assistance of a Master) a competent knowledge with ease and precision.

We humbly hope it will merit the approbation of those Gentlemen who have interested themselves in behalf of our endeavours, to whom we return our most sincere thanks, and are, with the utmost esteem and respect,

Their's and the Public's most obliged,

And obedient, bumble servants,

THOMAS and JAMES HARRISON.

PREFACE

Which we consider the utility of observations to mariners in general, and to those that trade into foreign parts in general, and to those that trade into foreign parts in particular, we need not be depicted to the particular of things in blead depicted for the particular of the particular to bring this blead on the particular trade of the particular fallows the coverance, we to note that one under our and excite the trade of the particular trade of the particular trade of the particular trade of the particular trade of the product of the position of the particular trade of th

We how hope it will meric the opposition of those considered the mission of those density outs, so whom we retain a out would find than to dark the winter than a creation out would find the core than the creation of the core than the core t



THE ROOM PERFECTS

THE

COMPLETE OBSERVATOR.

CHAP. I.

To find the Latitude of a Place, from the greatest Meridian Altitude of any Cælestial Body.

RULE.

If the zenith distance and declination be of one name, their difference is the latitude; if not, their sum is the latitude of the same name with the declination, except when the declination is subtracted from the zenith distance: but if the zenith distance and declination of the object be of different names, it is evident that the object must be between the zenith and equator. The distance between the zenith and the equator, or latitude, must therefore be equal to the zenith distance of the object added to its declination; and because the zenith lies on the same side of the equator as the object, the latitude will always be of the same name with the declination.

There are but four cases, or varieties, in working of observations by the Sun's meridian altitude, in whatsoever part of the world you are in, or whether the Sun's declination be North or South.

The first is, when the Sun is between the horizon and the equator; and then the RULE is, subtract the declination from the zenith; distance the remainder is the latitude of the place.

EXAMPLE.

EXAMPLE.

Suppose the Sun's zenith distance 76°; and the Sun's declination 16° South, what is the latitude?

N. B. The zenith distance is found by subtracting the corrected altitude from 90°, the remainder is the zenith distance.

The second is, when the Sun is between the equator and zenith; then the RULE is, add the Sun's declination to his zenith distance; the sum is the latitude of the place.

EXAMPLE.

Being at fea 27th of May, 1786, the Sun's meridian altitude was found 57° 35, and it was fouth of me; what was the latitude of the place?

The third variety is, when the Sun is between the zenith and elevated pole; then the Rule is, subtract the zenith distance from the Sun's declination; the remainder is the latitude required.

EXAMPLE.

Being at sea 14th of January, 1784, the Sun's meridian altitude was found 72° 17'S. what was the latitude of the place?

Meridian altitude	•	•	90 72	17	
Zenith distance - Declination -		-	17	43	South South
Latitude -	Opt G		-		South

The

The fourth variety is, when the Sun or star is between the elevated pole and the horizon; and then the RULE is, subtract the complement of the Sun's declination from the zenith distance; the remainder is the complement of the latitude.

EXAMPLE.

Being at sea July 12th, 1787, the Sun's declination 22° 00, and his corrected altitude was found to be = 05°; require the latitude?

0 01 -1				9'0°	
Sun's altitude	-		-	05	The Constitution of
Zenith -	-		-	85	distance
Complement	-	-	-	68	sun declin.
Complement	-	-	-	17	of latitude
Stoon of the second				90	
The court of the state of the s	+1	3 101	200		T J.
11:00:00:00:00				73	Latitude

But because it seldom happens that any sail so far North or South, as that they can conveniently take a backward observation by the Sun, under the elevated pole; in such case it may be done by forward observation, and work with the Sun's altitude or height above the horizon; and then the Rule is, add the Sun's altitude to the complement of the Sun's declination; the sum is the latitude; thus

The same operations will hold good in taking an observation by a star or planet.

In using an Hadley's Quadrant the Sun's altitude must be corrected for dip, refraction, and Sun's semidiameter.

EXAMPLE.

By a fore observation the altitude of the Sun's lower edge was taken and found to be 40° 20' South of the observer, when his declination was 9° 56' North; the eye being 30 feet above the horizon; require his true meridian altitude and latitude observed in?

THE COMPLETE OBSERVATOR.

Obs. alt. Sun's lower edge - Semidiameter to be added -	-	300 0 200 Au	2'0 S 16
App. alt. Sun's centre Dip of the horizon, to be subtr.	-	5.00	36
App. alt. cor. by the dip - Refraction to be subtracted	-	40	TOTAL PROPERTY.
True altitude Sun's centre True zenith distance Declination add	-	40 49 9	30 30 56 N
Latitude	-	59	26

By a back observation with Hadley's Quadrant, suppose the apparent altitude of the Sun's upper edge was taken 25° 12' South, when his declination was 21° 14' South, the eye 40 feet above the horizon; in what latitude was the observation made?

By observation alt Semidiameter to be subtr.		25°		
App. Sun's cen. of the Sun Dip of horizon to be added	-		56	Si
App. altitude cor. by dip Refraction to be subtracted	-	1100000	02	
True altitude of Sun's centre True zenith distance Declination		25 65 21	00	8
Latitude, North -	-	43	46	

To find the Latitude by the Meridian Altitude of the Moon.

FIND the time of the Moon passing over the meridian of Greenwich in the ephemeris, to which apply the longitude of the ship or place, turned into time by Addition or Subtraction, according as the place is E. or W. which call the reduced time.

To this time find the Moon's semidiameter and horizontal parallax in the ephemeris for the month.

Correct

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Correct the observed altitude for her semidiameter, dip, &c. to which add the correction for her observed altitude and horizontal parallax, and you will have her true altitude—hence the latitude as before.

To find the Latitude by the Meridian Altitude of any of the Planets.

IN the Nautical Almanack, find the time of the planet passing the meridian of Greenwich; reduce this time to the meridian of the ship; then having the altitude and declination, the latitude is found as by a fixed star, or the Sun.

ewi sal mast so sans C H A P. II.

The Method of finding the Latitude from the Observation of two Altitudes of the Sun, and the Time between each Altitude.

Cautions which relate to the proper times for making observations.

THE two observations must always be taken between nine in the morning and three in the afternoon, if possible; but, the nearer they are to noon, the truer your latitude, provided there be a sufficient interval between them. The following directions will be of use to shew what interval is proper.

If both altitudes are taken in the forenoon, the interval between them must not be much less than half the distance of the first altitude from noon.

If both altitudes are taken in the afternoon, the interval of time between them must not be much less than the first altitude from noon.

If one altitude was taken in the forenoon, and the other in the afternoon, the interval of time between them must not exceed four hours and a half.

These cautions will give the Mariner sufficient reason to see there are many exceptions to the finding the latitude by two altitudes; and the same is attended with much trouble; I therefore think the method to find the latitude by one altitude only, (at any hour of the day) preferable; but that the

Mariner may be properly instructed how to find the same by two altitudes, the following Rules will sufficiently qualify him to perform the same.

RULES.

- I. Find the arithmetical complement of the logarithm, co. fine of latitude by account, add the arithmetical complement of the logarithm co-fine of the Sun's declination: call their fum the log. ratio.
- II. From the natural fine of the greatest altitude, subtract the natural fine of the least altitude; find the logarithm of their difference, and write it under log. ratio.
- III. With half the elapsed time under Table 4, and from the column of half the elapsed time, take out the logarithm answering thereunto, which is also to be set down under log. ratio.

It is sufficiently correct (for common use) to take the time to half a minute, but if greater accuracy be required, the difference between the two nearest logarithms must be applied.

- IV. Add these three logarithms together, and with their sum enter the table in the column of the middle line; where having found the logarithm nearest thereto, take out the time corresponding to it, and put it down under half the elapsed time; subtract the lesser from the greater, their difference will be the time from noon, when the greatest altitude was taken.
- V. With this time enter the table; and from the column of log. rifing, take out logarithm corresponding thereto: from this logarithm of a natural number, which, being found in the common table of logarithms, and added to the natural fine of the greatest altitude, will give the natural fine of the meridian altitude of the Sun.

From the meridian altitude of the Sun, the latitude is eafily obtained by the rules for finding the same at the beginning of this book.

N. B. If the latitude found by this process should differ widely from the latitude by account, it will be proper to repeat the operation, using the latitude last found instead of the latitude by account, till the result gives a latitude nearly agreeing with the latitude used in the computation.

EXAMPLES.

EXAMPLES.

Being at fea in the latitude of 47° 19', by account, when the Sun's declination was 12° 16' N. at 10 h. 24' A. M. per watch, the Sun's altitude was found 49° 09', and at 1 h. 14' P. M. per watch, his altitude was found 51° 59': require the true latitude?

		Time		Al	tit.				
2.956.20	H.	M. 24.	S.		M.	Nat. fin 75642	es S. dec.	47° 1	'90.16880 60.01003
105450	ı.	14.	00	51.	59	78783	log. rat	4	0.17883
Elap. time		50. 25.	00	its log.	in col.	of balf	its loga elap. time	r. o	3.49707
A Comment	0.	15.	00	in col.	of M.	T. correj	sponding t	0	4.11667
Time at noon Ditto per watch	I. I.	10.	00	its log.	from	col. of I	log. rati	5	3.66542 0.17883
Watch fast	0.	4.	00			num. of	this log.	aleib proper	3.48659
Sun mer. alt. Sun's Sun's dec.	35.	56° 4 16	201	8184 nith dista		. fine of	Sun's mer	. alt.	
Latitude	47.	20	in	North				U.H	

Here the latitude, found by computation, may be relied on, as it differs only one mile from the latitude used in the operation. It is hardly necessary to observe, that by the Sun's altitude is always meant its correct altitude.

EXAMPLE II.

Being at sea, in latitude by account 50° 40' North, when the Sun's declination was 20° 00' South, at 10 h. 17' A. M. per watch, the Sun's altitude was taken 17° 13', and at 11 h. 17' A. M. per watch, it was taken 19° 41': require the true latitude?

Times

es and a second	H.	M. 17.	S.	Alt. D. M. Nat. fines 17. 13 = 29599	D. M. Lat. 50. 40- S. dec. 20. 00-	-0.19803
antitude was	II.	17.	00	19. 41 = 33682	Log. rat.	0.22504
Elap. time		oo. 30.		4083	be true letitude ?	3.61098 0.88430
	ı.	ı.	00	in col. of M. T. correspond	onding	4.72032
Time from noon Ditto per watch		31. 43.		100 . 00 . 75 Miles	10. 24. 00	2.95529
Watch flow	0.	12.	00	538 33682	m ", 50 00	2.73025
The second second	Natu	ral	fine !	Sun's mer. alt. 21220 =	20° 01' = Sun's	alt.

Natural fine Sun's mer. alt. 34220 = 20°. 01' = Sun's alt.
69. 59 Sun's zen. dist.
20. 00 Sun's dec.
49. 59 Latitude.

As the latitude, by this computation, differs 41' miles from that by account, it is proper to repeat the operation, using the last-found latitude, in-stead of that by account.

	of Sant's marray	D. M. 12. A	Sun mer, al.
		49. 59	0.19178
		20, 00	0.02701
	H. M. S.	Log. ratio	0.21879
Half elap.	o. 30. 00 time		0.88430
as id differs	1. 00. 00	latitude, found by computation	
A STATE OF THE STATE OF		lle from the lained wist indher that by me Bon's abilited is an	
• • • • • • • • • • • • • • • • • • • •	0. 30. 00	an algeritus baller in the forest	2.93223
	0. 43. 00		0.21879
Watch flow	0. 13. 00	I TSIN A X I	2.71344
		33682 D. M.	, 311
	of Mental whien the		in Guraci
	via per wreigh, the Si per watch, it was tel	0.00	and in
· The Garage	con cover in elleration and	70. 00 = Sun's de	
CHIEF		50. 00 Latitude	The state of the s

The latitude last found, differing only one mile from that used in the operation, may be relied on as the true latitude.

EXAMPLE

EXAMPLE III.

Being at sea in latitude, by account, 60° o', when the sun had no declination; at 1 h. o' P. M. per watch, his altitude was 28° 53', and at 3 h. o' P. M. per watch, it was 20° 42': require the true latitude?

	Times H. M. S 1. 00. 0			Lat. Sun's dec.	60.		0.30103
	3. 00. 0	20. 4	12=35348		Log.	rat.	0.30103
¿ elap. time	2. 00. 0 I. 00. 0		12955				4.11244
	2. 00. 0	00					5.00047
Time from noon	1. 00. 0	0			Log.	rat.	3.53243
		4830					3.23140
		5000	6=30.00	Sun's mer. Latitude	alt.		

Here the latitude by computation comes out the same with the latitude by account, which shews that the latitude by account was right. From the foregoing examples it is plain that the operation is the same, whether the Sun has North or South declination, and will be the same whether the ship is in North or South latitude. It is also clear, that when the Sun has no declination, the arithmetical complement of the log. co-sine of the latitude is the log. ratio.

Hereto it has been supposed that both the altitudes were taken at the same place or station; but as that can seldom happen at sea, the necessary corrections for any alterations in your station may be readily made as follows:

Let the bearing of the Sun, at the instant of the first observation, be taken by the compass, which call the Sun's bearing; and when the second observation is taken, find how far the ship has gone, in the time between the observations, towards or from that point of the horizon in which the ship hath gone, in the time. This quantity added to the aforesaid altitude, if the ship hath moved towards the aforesaid point, or right subtracted from the first D altitude,

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altitude, if the ship hath gone farther from the said point, will reduce the first altitude to what it would have been found, if observed at the same station where the second altitude was taken.

Thus suppose that when the Sun bore S. E. ½ E. by the compass, his altitude was observed 18° 27'; and three hours after, it was observed 38° 23'; the ship in the mean-time having gone S. E. ½ E. by the compass, at the rate of 6 knots per hour: require what the first altitude would have been found if it had been taken at the same place as the second was?

Here the ship's course was directly towards that point of the horizon the Sun bore on when the first altitude was taken; the whole distance run between the altitudes being 18' miles, must be added to the first altitude, which will make it what it would have been if it had been taken at the second station; so that the two altitudes for finding the latitude at the last station will be found 18° 45' and 38° 23'.

But if the ship had sailed N. W. ½ W. or directly from the point that the Sun bore on at the time of the first altitude, in such a case the 18 miles must have been subtracted from the first altitude.

When the ship's course makes an obtuse or an acute angle with the Sun's bearing, the distance gone towards, or from, that point that the Sun bore on, may be readily sound by the help of the Tables of Difference of Latitude and Departure.

Thus suppose, that when the Sun bore S. E. b. S. by the compass, the altitude was taken 26° 50'; and after sailing 18 miles on a South course by the compass, his altitude was taken 37° 10': require what the first altitude would have been if it had been taken at the second station?

Here the ship's course, making an angle of 3 points, or 33° 45' with the Sun's bearing, find in the Table of Difference of Latitude and Departure what the difference of latitude will be when its course is 3 points, and distance 18 miles, and you will find 15 miles to be added to the first altitude, the ship having gone so much towards the point the Sun bore on; so that the two altitudes to be used at the second station for finding the latitude will be 27° 05 and 37° 10.

Had the ship's course been North, or 3 points from the point opposite to the Sun's bearing, in that case the 15 miles must have been subtracted from the first altitude.

When the ship's course is at right angles, or eight points from it, such cases need no correction.

EXAMPLE.

EXAMPLE.

Suppose a ship at 9 h. 55' 30" A. M. per watch, observes the altitude of the Sun to be 17° 33' South, viz. bearing S. b. E. ½ E; then sails 7 knots per hour, on an E. ½ S. course, by the compass, and at o. h. 54' 10" P. M. per watch took the Sun's altitude 21° 55': require the latitude of the ship, when the last altitude was taken, the declination of the Sun being 19° 30' South, and the latitude, by account, being 47° 34' North?

The ship's course, in this case, makes an angle with the bearing of the Sun of 64' points, and the distance run between the altitudes is 21 miles; therefore from the Tables of Difference and Departure, the difference of latitude answering the course and distance = 7 miles to be added to the first altitude, the ship having gone so much towards the point of the horizon the Sun then bore upon; so the two altitudes to be used for finding the latitude of the last station are 17° 40' and 21° 55'.

SIST YES	Cor.	17° 33′ ×7 Na	t. sines			D. M. 47· 34	0.17087
	н. м.	S.	17. 40=	= 30348 S.	dec.	19. 30	0.02565
and the role	9. 55.	30	21. 55	37326		Log. ratio	0.19652
sa site mid	0. 54.	10		6978			3.84373
sult accessed	2. 58.	40					
telap. time	1. 29.	30					0.41945
- 20 30 3	o. 33·	00					4.45970
Time from noon Ditto per watch							3.47282
Watch slow Natural sine			ltitude	1889 37326	D.	M.	3.27630
Natural fine	of the S	Sun's mer	rid. alt.	39215 =	23. 66. 19.	o5 M. A. 55 Sun's zen. 30 Sun's dec. 25 Latitude	dist.

C H A P. III.

To find the Apparent Time at Sea, and thereby regulate the Going of the Watch.

A MONG the many methods proposed for this purpose, that of equal altitudes seems the easiest to practise at sea. At the time when you think the watch stands in need of being regulated for an observation for finding the latitude at any hour of the day, by a single altitude, let the Sun's altitude be taken at any convenient time in the forenoon; set down the time and altitude; in the afternoon wait for the Sun having the same altitude exactly you had in the forenoon, and note down the times; then half the sum of those times is the apparent time shewn by the watch when the Sun was upon the meridian of the place.

Lest the altitude taken in the forenoon cannot have a corresponding one in the afternoon, by the interposition of clouds, it is therefore proper to take several in the forenoon, in order to have a greater probability of securing a corresponding one in the afternoon; and if several observations of equal altitudes can be taken on both sides the meridian, it will be best to find the noon for each pair, and take the mean of all for the true one.

And if there is reason to believe the watch gains or loses considerably in a day, other sets of altitudes, on successive days, may be taken, whereby the daily variation of the watch may be known and allowed, by which means the artist will have nothing more to do in finding the latitude, by one altitude, than allowing what the watch gains or loses in a day, and the equation of time between the Sun and watch, and the latitude may be depended upon as true as any meridian altitude.

The altitudes should be taken in the same place, if possible; but if the ship cannot lie by the same, rules must be observed, what point the Sun bore upon when the first altitude was taken; and find the difference of latitude the ship has made since the first altitude was taken, by the Tables of Difference of Latitude and Departures, and add or subtract that difference as before directed.

EXAMPLE.

To fine the Latitude of

Time of the Day, a

A. S froc complement of

much from the South, 'Il v

EXAMPLE.

March 1st, 1787, at 8 h. 40 m. in the forenoon, and at 3 h. 16 m. in the afternoon, the Sun had equal altitudes: require the going of the watch?

H. 8 12 3	M. 40 00 16	add together
1/2)23	56	I U U I
11	58	ence be altinided to tech
6	02	watch too fast

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het, if won are

000245

19.00 42

0.88061

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Take notice, when the watch is fast, the half sum is less than 12 hours; when slow, then the half sum is more than twelve; when right, just twelve hours.

E X A M P L E H. H. on the shift of

Feb. 28th, 1787, in latitude 54° 30' North, at 8 h. 10 m. in the forenoon, and at 3 h. 58 m. I had equal altitudes of the Sun: how did the watch then go?

E X A MIP LINE all. Apolo or med all

April 24th, 1787, being at sea, and had at 10 h. 30 m. and 1 h. 30 m. equal altitudes: require the going of the watch?

being fibrisded from sunf dolaw : 00' on's I'm azimuth from the

C H A P. IV.

To find the Latitude of a Place, by one Altitude only, at any Time of the Day, when the Sun is above the Horizon, and can be seen.

RULES.

As fine complement of the altitude is to the fine of the hour from noon, fo is fine complement of Sun's declination to fine of the Sun's azimuth from the South, (if you are in the North altitude; but, if you are in South latitude, from the North) which being taken from 180°, gives you the azimuth from the North, if your latitude be North; but, if South, it gives the azimuth from the South. Then you have in the oblique spherical triangle two sides and two angles given, to find the other side, which may be solved as follows, viz. As the sine of ½ the difference of the azimuth (of the same name with the latitude) and hour from noon is to the sine of their ½ sum, so is the tangent of ½ the difference of the complement of the altitude and complement of declination to the tangent of ½ the complement of the latitude; which, being doubled, will give you the complement of the latitude; and that taken from 90°, will give you the latitude of the place: and if your watch can be depended upon, and properly corrected by a table, intitled, A Table of Clock or Sun, it will give you the latitude as true as any meridian altitude, and a little practife will make it as easy.

EXAMPLE I.

June 21st, 1785, at 38" past 10 in the morning, per watch, I took the Sun's altitude 53° 45', what was the latitude of the place? By comparing the watch with equation of time, it is found 38" too fast, therefore it is by the Sun 10 o'clock in the morning: Then,

As S. C. of altitude 53°.	45	1787, 00	9.77181
is to S. of the bour from noon 30.	001	H	5 9.69847
So is S. C. of declination 66.	3100	01	1 9.96245
and together	300	. 21	19.66 42
to S. of Sun's azim. from South 50.	5108	1	9.77181
	00	42(2	9.88961

Which, being subtracted from 180°, gives 129° .09', the azimuth from the North.

Hour from noon	129° .09′ .00′ 30 .00	Š.
Difference is Half their difference	99 .09 49 .34 .30	
Sum of the azimuth and hour from noon	1)159° .09'	
Half their sum	79° ·34′ ·39	<u>''</u>
Complement of altitude Complement of declination	36° 15'	an sail
Difference	1)30 16	in Targer
Half their difference	15 8	1/4/2
Then As S. of ½ the difference of azim. and hour from noon is to S. of their ½ fum so is T. of ½ the difference of co. of alt. and co. dep.	49° ·34′ ·30″ 79 ·34 ·30 15 .08	9.88198 9.99277 9.43708
to T. of ½ the com. of latitude 2 Complement Doubled	19 .14 19 .14 2	9.54287
Gives complement of latitude Subtracted from	38 .28	
Gives latitude in	51 .32	The terms

EXAMPLE II.

Being on the North sea, January 9, 1785, I observed the Sun's altitude at 7' 38" past 8 in the morning 1° 14', and his declination that day was 20 11' South: require the latitude?

Now, by comparing the watch with the equation of time, I find it 7' 38" too fast; therefore by the Sun it is just 8 in the morning.

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As S. C. of altitude	88° .46′	9.99990
is to S. of hour from noon fo is S. C. of declination	60 .00 69 .49	9·93753 9·97248
igo. *et (1 } ***	Sun of the cal	9.99990
to S. of Sun's azim. from the Sou	tb 54 .24	9.91011
Taken from 180° leaves 125° The azimuth from the North Hour from noon	36' 125° .36' 60 .00	3
Difference Half their difference	65 .36 32 .48	
Sum of the azim. and hour }	185 .36	FOOT
Half their sum	92 .48	azon, and b
Complement of altitude Sun's distance from the North	88 .46 pole 110 .11	to S. of their is T. of their
Difference Half their difference Then	10°.42′.	30"
As S. & difference of azim. and b	our } 32° .48′	9.7337
is to S. \(\frac{1}{2}\) their fum fo is T. of \(\frac{1}{2}\) difference of com. of alti. and com. of declin.	92 .48	9.9994 30'' 9.2766
The state of the s	i i i i i i i i i i i i i i i i i i i	19.2761
To T. com. of i of latitude	19 .14 12 fea. Januar	9.5424
Complement of latitude Subtracted from	38 .28	pell 3 in the
Gives the latitude in	51. 32	as before

EXAMPLE

EXAMPLE III.

March 20, 1782, I took the Sun's altitude at 7 in the morning, (when my watch was properly adjusted by the Table of Equation of Time) and found it 9° 16', when I had made proper allowance for refraction and the height of my eye above the surface of the water; from which the latitude is required?

As S. C. of altitude	9°	16'	9.99429
is to S. of hour from noon fo S. C. of declination	75 90	.0	9.98494
to S. of the az. from the South	SHI	.10	9.99065

	to S. of the az. from the South	78	.10	9.990	65
78	10' taken from 180° gives the azir Azimuth from the North Hour from noon	muth fro	m the 50'	North.	Then,
	Their difference Half their difference	26 13	50 25		
	Their sum Half their sum	176	50		
	Complement of altitude Complement of declination	80	44		
	Their difference Half their difference	9	16 38		
	100.1 " 0.1 "	THE RESERVE			

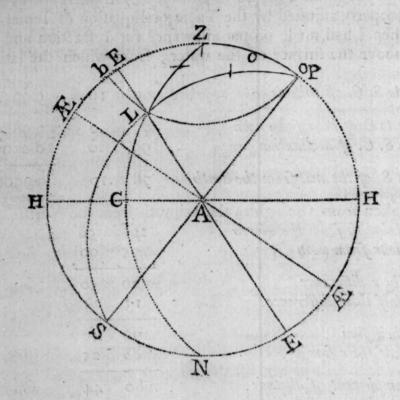
As S. of the diff. of the azi. and hour from noon	13	25	9.36555
is to S. of their & fum	88	25	9.99983
fo is T. of \(\frac{1}{2}\) the differ. of the \(\frac{1}{2}\)	4	38	8.90872

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es clareds on the promitive tirele from the h	18.90855
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to T. com. of 1 the latitude 10° 14'	0.54200

uming his amon actual of spirit	2 11 -
Doubled is the com. of the which subtracted from	38° 28 Lat. 90 00 gives
Latitude by observation	51 32 as before

uosino

A Harriede



To find the Latitude by Projection.

To construct the problem geometrically, you must find the azimuth from the South, which subtracted from 180° leaves you the azimuth from the North; then with its complement taken from the half tangents, set from the centre A to C, draw the oblique circle Z C N; then set off the altitude of the sun, from the chords on the primitive circle from the horizon H H towards Z to cut the primitive circle in b and o, and draw the parallel of altitude b o, and where the parallel cuts the azimuth as at L; then thro' L and A draw the ecliptic E Æ; then from the ecliptic towards H, set the declination, if North; but if South, towards Z; then draw the equinoctial, and at right angles thereunto draw the poles P S, and draw the oblique circle P L S, and it is done; for P Z is the complement of latitude, and P H is the latitude of the place.

C H A P. V.

To correct the Going of the Watch by another Method.

To make requisite computations.

PROBLEM I.

TO find the apparent time from an observed altitude of the Sun, the latitude of the place being known, as here, as we suppose, the latitude by dead reckoning.

SOLUTION.

If the latitude and the Sun's declination be of the same name, take the declination from 90°, but if the latitude and Sun's declination be of different names, add the declination to 90°, the difference or sum is the Sun's polar distance.

Find the co. latitude, and the Sun's co. altitude.

Add into one sum, the polar distance, co. latitude and co. altitude; take half the sum; find the difference between the half sum and the co. altitude.

Add into one fum, the arithmetical complement of the log. fine of the co. latitude, the arithmetical complement of the log. fine of the polar distance, the log. fine of half the sum, and the log. fine of the difference, take half this sum: this last half sum is the co. sine of an angle, which being doubled, is the Sun's horary angle. The horary angle turned into time, will give you the instant of observation from noon. If the Sun be rising, or on the East side of the meridian, take this time from twelve hours; and the remainder is the time of observation; but if the Sun be on the West of noon, this time is the instant of observation.

EXAMPLE I.

In latitude 51 32' North, by account, June 21, 1786, at 10 in the morning, by my watch, I observed the Sun's lower limb 53° 31': require the L. time, and error in the watch?

					THE PERSON N	Filler Co. Section 19	St. 201 12 1 1 1980
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	History of States of State		Marine & HOLD on	مالك حالت دالك			

Sun's altitude ×Semi-fub. Altitude of Sun corrected Co. altitude Co. latitude Co. declination	36	14 ·45 .15	C Goin	To correct the
Polar distance Co. latitude Co. altitude	38	28	To m P R	0.03749 0.20617
ersum is no solution borns	141	15	tiod son	O find the appear
Half sum Sum Co. altitude	7° 34	37 22	30	9.75174
be of the fame name, take	goizenilos	a's de	Sum	bn 19.97008 ada 11
Sun's declination be of decence or fum is the Sun	bins shift	3	it it it antion t	19.97008
Dev. U.J		6		

150 converted into time gives 10 h. 0 m. 24" and 12 h. leaves 1 h. 59 m. 36": time when the observation was made 10 in the morning per watch, Thew the watch 24" flow. half the fum; find the differen

- 31 - 3il

EXAMP LE H.

Being on the North sea January 9, 1785, I observed the Sun's altitude 1° 14' I found my watch exactly 8 in the morning: I require the true time of observation and error in the watch?—Rule as by former Rule.

o time, will give you	ndi hoared	10	14' 46	51° 3	2'	22°	08'
ming, or on the Euc.	s Sun be a	88	46	38 2	8	112	08
: and the remainder	empari sais	WI BIS	off curit	se this	MI AN	arbiner.	G (241)

VI introduo la mantal chi si A P. CH

To find the Latitude without knowing the Sun's Declination; and if the Day of the Month be loft, how to know what Day the Observation is made.

HIS may be done in any latitude, whose complement is less than the Sun's declination on the fame fide of the line the place of observation is on; for the Sun will be twice upon the meridian in twenty-four hours, viz. above the pole at noon, and under the pole at midnight.

RULE.

RULE.

To find the latitude without knowing the Sun's declination, take the Sun's altitude at noon, when above the pole, and at midnight, when under the pole; half their difference is the complement of the latitude of observation.

EXAMPLE.

June 21, 1786, I took the altitude of the Sun in Greenland, when on the meridian above the pole 33° 28', and at midnight under the pole 13° 28', what was the latitude of the place?

Altitude above the pole Do. below the pole	33°	28' 28
Half their difference	1/2)20	00
Complement of latitude	10	00
Complement of latitude Latitude of observation	80	00

To find the day of observation, and thereby know the day of the month, this is the Rule: add the two altitudes together, half their sum is the Sun's declination for the day of observation.

EXAMPLE.

In the year 1786, I took the Sun's altitude in Greenland, when on the meridian above the pole 33° 28', and at midnight under the pole 13° 28': what time in the year was the observation made?

Sun's altitude above the pole Sun's altitude under the pole	33° .28′ 13 .28
Sum .	1)46 .56
Half their sum shews the day to be June 21st.	23 .28

N. B. It is here supposed the two altitudes are taken in the same place; and likewise they are to be the corrected altitudes, if taken by an Hadley's Quadrant.

CHAP.

C H A P. VII.

The Method of finding the Longitude from the Observation of the angular Distance between the Moon and the Sun, or a fixed Star.

HE motion of the Moon being much quicker than any other celestial body, is the reason why its angular distance is much better adapted to discover small differences of time, than like observations made with any other body. The method of observing its place at sea is, that of measuring the angular distance between it and the Sun, or a fixed star. This being done, it is plain, if by means of an ephemeris, the time of Greenwich corresponding with the observed distance, be found the time at the place of observation; being likewise known, the difference between these two times being turned into degrees and minutes, will give the difference of longitude between Greenwich and place of observation.

The calculations in the ephemeris being supposed to be accurate, the chief difficulty of this method will consist in finding the correctings necessary to be applied to the observed distance, to give the true distance as it would appear if taken at the centre of the earth. For since the altitude of every celestial body, not in the zenith, is rendered apparently greater by refractory power of the atmosphere, and is likewise apparently diminished by the parallax, it scarcely ever happens that the observed distance is equal to the true distance; but the very great distance of fixed stars renders their parallax absolutely insensible; and the horizontal parallax of the Sun being about $8\frac{2}{3}$ seconds, is seldom considered in practice.

Because the quantity of refraction and parallax depends on the altitude, it is necessary, in order to obtain the quantities, that the altitudes of both the objects should be taken at the same time that the angular distance is measured. A set of observations can be taken by no less number than three perfons.

To make the requisite Observations.

First, To find the apparent time at the place of observation: This is most conveniently done by taking one or more altitudes of the Sun, and noting the time by a good watch: from each observation, compute the time; the difference between this time, and the correspondent time, noted by the watch, will shew how much the watch is fast or slow.

The

The mean of feveral observations, in all cases where it can be had, is always to be preferred. The best time to take the Sun's altitude for the solution of this problem, is when the altitude changes quickest, and this is when the Sun bears East or West.

Secondly, To make the observation of distance: The three observers being in readiness with their instrument carefully adjusted, according as directed, and the watch being suspended near one of the observers, or put into a fourth person's hand, appointed to note the time, two of the observers must take the altitudes, while the third measures the distance; and take notice, that in all cases the convex or exterior well defined edge or limb of the moon, must be used or brought to the horizon, whether that edge uppermost or lower limb of the Moon.

In measuring the distance, the most obscure or least luminous of the two objects must be viewed directly, and the other must be brought, by reflection, into the apparent contact with it. In this case also, the well defined edge of the Moon must always be made use of for the contact, even though it should be necessary, for that purpose, to make the reflected image pass beyond the other. In the night time it will be found advantageous to turn down one or more of the green screens, in order to take off the glare of the Moon, which would otherwise prevent the star from being seen. As soon as the observer of distance has settled his instrument to the required angle, let him give notice to his affiftants, who, that moment must read of the respective altitudes from their quadrants; at the fame instant, the fourth observer, or one of the three, as previously fettled, notes the time by the watch. These four particulars being wrote down with expedition, the fame observations are to be again repeated in the same manner, and the setts respectively wrote beneath the others. After fix or feven fetts have been made, the mean of the whole must be taken, from whence the longitude must be found by computation. If the watch made use of here be a stop watch, the time will be more to be depended upon, because the watch may be stopped the instant the obferver finishes his distance, and the watch may be set to the exact time again by another time-piece, before the observers again repeat the operation, which must be done as soon as convenient.

PROBLEM I.

The apparent distance of the centre of the Moon, from the centre of the Sun or a fixed star, together with their respective apparent altitudes, to find the corrected distance as it would appear if beheld from the centre of the earth.

R U L E S.

I. Find the respective co. altitudes; place beneath each other the apparent distance of the Sun or star's co. altitude, and the Moon's co. altitude. Find their sum, and half sum, and also the difference between sum and half sum of the Sun or star's co. altitude. Add together the ar. co. log. sine of the apparent distance, the ar. co. log. sine of the Moon's co. altitude, and the log-sines of the half sum, and of the difference. Half this sum, and it will be log-co. sine of an angle, which being doubled gives the angle at the Moon.

II. Find, as above, the sum and half the sum of the apparent distance, the Moon's altitude, the Sun or star's co. altitude: find also the difference between the half sum and the Moon's co. altitude; add together the ar. co. log. sine of the apparent distance, the ar. co. log. sine of the Sun or star's co. altitude, and the log. sines of half the sum, and of the difference; half this sum, and the half will be the log. co. sine of an angle, which being doubled, gives the angle at the Sun and star.

III. Then fay, radius, fine co. Moon's altitude: * horizontal parallax; parallax in altitude: from the parallax in altitude, take the refraction found in the Table of Refraction, corresponding to the Moon's altitude; the remainder is the error of the Moon's altitude.

IV. Radius: fine co. of angle at the Moon's: error of the Moon's altitude: is first error in dist. which is to be added the apparent distance, if the angle at the Moon be obtuse, but otherwise subtract.

V. Radius to fine co. of the angle of at the Sun or star: refraction corresponding to the Sun or star's altitude: second error in distance, which add to the apparent distance, if the angle of at the Sun or star be acute, otherwise subtract.

From the corrected distance, to find the longitude of the place observed in: feek, in the ephemeris, on the day of the month, for the two computed distances nearest the distance observed; find the difference between the two computed distances, which call the first difference; find also the difference between the earliest of the two computed distances, and the correct observed distance, which call the second difference: then say, as the first difference: second difference: 3 hours: a proportion of time, which added to the time of the first of the two computed distances, gives the apparent time at Greenwich;

^{*} The Moon's borizontal parallax is found in the Nautical Ephemeris, against the day of the month.

Every other element used in this computation, besides the angles, ought to be taken from that work.

EXAMPLE.

Suppose the following observations be taken in latitude 34. 17' N. and longitude by dead reckoning 13° 56' West of Greenwich, height of the eye 18 feet: it is required to compute the true longitude from the same.

		ril 4th, ne by w		The second second	nce obi		Obse altitu sun's limb horiz the s	de of low. from con of	Obfe altitu moon' limb the he of the	de of slow. from oriz.
	h.	m.	S	•	•	"	0	· ·	•	
	4 4 4	47 50 55	14 11 26	73 73 73	41 43 47	53 55 33	22 22 21	50 12 6	80 80 81	17 36 9
s.	14	32	51	221	13	21	66	8	242	2
M.	4	50	57	73	44	27	22	3	80	41

The going of the watch must be ascertained from the method for correcting the same by the RULES aforegoing. By such observation we here suppose it to be known that the watch is 22 m. 38 sec. too fast, therefore 4h. 50' 57"-22' 38" gives 4h. 28' 19" the apparent time of observation. Previous to the actual computation for clearing the distance, it will be necessary to reduce the feveral observations to the centre of the Sun and Moon: feek in the ephemeris for the femidiameters of the Sun and Moon for the time of obfervation: the semidiameter of the Sun is 16' 1", and that of the Moon for noon at Greenwich is 15' 22", and for midnight 15' 16": now the difference of time equivalent is 13° 56' West of Greenwich, is about an hour, which added to the observed time 4½ hours makes 5½ hours for the time roughly estimated for Greenwich. The difference of the Moon's semidiameter for 12 hours, is fix feconds; therefore 12 h. :: 6": 51 h: 21", which as the semidiameter is decreasing must be taken from 15' 22", and leaves 15' 19'' for the Moon's semidiameter at the time of observation. This is the Moon's semidiameter as it would be if it was seen from the centre of the earth. To 15' 194" add 16" for the increasing arising from the Moon's altitude, and the correcting the femidiameter; rejecting the " will be 15' 35" to bring the observed distance of the nearer limbs of the Sun and Moon to the apparent distance of their centres, the semidiameter of each must be added: That is 73° 44' 27'' + 16' 1'' + 15' $35'' = 74^{\circ}$ 16' 3'' = the apparent distance of the Sun and Moon's centres.

and the day of the day

To find the apparent altitude of the Sun's centre, the femidiameter must be added, and the dip subtracted; that is $22^{\circ}3' + 16' - 4' = 22^{\circ}15' =$ the apparent altitude of the Sun: it is not necessary in the altitudes to proceed to seconds.

To find the apparent altitude of the Moon, the lower limb being found used, the semidiameter must be added, and the dip subtracted; that is 80° 41' + 16'-4' = 80° 53'; the apparent altitude of Moon. In like manner as the Moon's semidiameter was sound for the time of observation, so also must the horizontal parallax. Now the horizontal parallax at noon 56' 24"; and at midnight 56' 1", the difference 23". Therefore 12 h.: 23":: 52'h. 11", which subtract from 56' 4", because the parallax is decreasing leaves 56' 13", for the horizontal parallax at the time of observation. This expressed in minutes and decimal parts 56'. 217: with these data we proceed according to the problem.

according to the problem		
	Sun's app. alt. 2	2° .15′
	com. of alt.	7 .45
	Moon's app. alt. 8	0.53
Server vol bontage of	com. alt.	9 .07
App dif. 74° .16'	Arit. co. fine	0.01658
Moon'sco. alt. 9 .07	Arit. co. fine	0.80012
Sun's co. alt. 67 .45	Mittaliana Managara	the artent computation
Sum 151 .08	Attended to Some for mean	the saveral observation
Half 75 .34	Sine	9.98607
Diff. 7 .49	Sine	9.13355
	AND WEST OF THE STATE	19.93632
Said ed Salance	Co. fine	9.96816
analigate theological	21° .40′	
Doubled	43 .20 = an angle at the M	Toon
Ap. dif.		01658
Sun's co. alt		03360
Moon's co. alt.	9 .07	the September 1 conditions
Sum	151 .08	real for the contract
Half	75 ·34 9	98607
Succession of the Spinsons	67 .27 9.	96223
	19	.99848
Doubled	3 .23 co. fine 9. 6 .46 = angle at the Sun	99924

As Radius : S. C. Lo alt. 80° .5'3 :: Horiz. parallax 56' .217	10.00000 9.19988 1.74987
: Par. in alt. Sub. ref. 15' 9" = 8' .91	0.94975
Error of Moon's alt. 8 .76 As radius 90 .00 : S. C. ang. at D 43 .20 :: Error D alt. 8' .76	10.00000 9.86176 0.94250
Error in dif. which \ 6' .37	0.80426
As radius 90° .00 : S. C. \(\alpha\) at Sun 6 .46 :: Ref. cor. to al. 2'20'' = 2 .333	9.99696 0.36791
: Second err. in dif. 2 .317 which must be added } 2 .317	0.36487

Now 6' 37 = 6' 22'' 12''' and 2' 317 = 2' 19'', whence the apparent diftance 74° 17' 3'' - 6' 22'' 11'' + 2' $19'' = 74^{\circ}$ 11'' 59'' 48''' = corrected diftance. By Lyon's Compendium, the correct distance comes out 74° 11' 58" and by Mr. Dunthorne's Compendium it is 74° 11' 50".

The same example by Gunter.

Radius : S. 74° 16' : : 9° 07' : S. 8° 46'.

S. 8° 46': S. 75° 34':: S. 7° 49': a fine opposite to which on the line of versed sines stands 4310 = the angle at the Moon.

Now,

Radius: S. 9° 07':: 56' 22": 8' 9=Par. in alt. from which take 15' refraction, and the remainder 8' 75", is the error of the Moon's altitude.

Radius: S. 74° 16':: S. 67° 45': S. 62° 50' S. 62° 50': S. 57° 34':: S. 66° 27' a fine opposite to which on the versed fines stands a point, which is rather to the left hand of the half division of the space between the beginning of the line, and the division of 10°; we shall therefore call it 6° = the angle at the Sun.

is the epiemeris the time the Moon or any of the P , bnA' centre Radius: S. C. $53\frac{1}{2}$ = S. $46\frac{1}{2}$: error of alt. 8' 75'': first error of dist. 6' $33'' = 6' \cdot 19'' \cdot 48'''$.

Radius

Radius: S. C. 6° = fine 84° : refrac. in alt. \bigcirc 2' 33: fecond error is dift. 2' 32 = 2' 19'' 12'''.

Laftly, 74° 16' 3'''—6' 19" 48''' + 2' 19" $12'' = 74^{\circ}$ 12' 02'' 24"' corrected diftance. The correct diftance 74° 11' 59" 48'', we will call 74° 12' because the 48''' may be taken as a whole second; Therefore,

Distance by the ephen				27"
at	6 do.			50
Observed distance		74	12	00
First difference	45. 0.4	1	27	23
Second difference		. 1	10	33

Now, 1° 27' 23": 1° 10' 33":: 3 h.: 2 h. 25' 19", which added to 3 h. gives 5 h. 25' 19" = the time at Greenwich.

The time at Greenwich

Time at ship

Difference of time

5b. 25' 19"

4 28 19

57 00

gives 14° 15' longitude, which is West, because the time at Greenwich does not proceed the time at the ship. If the distance, as given by Gunter, be used, the longitude will come out 14° 16 West. The longitude thus found, is the longitude of the place of observation; for the watch is here supposed to go true during the interval between the altitudes and distance.

N. B. If the Sun rifes or falls quick, the observation of distance it will be convenient to compute the time directly from the mean altitude.

C H A P. VIII.

A new, concise, easy, and infallible Method to determine the Longitude at Sea, independent of the dead Reckoning, by one Person only, and no other Instrument but an Hadley's Quadrant well adjusted.

R II I. F.

FIND in the ephemeris the time the Moon or any of the Planets' centres pass the meridian of Greenwich; take the time by the watch, well regulated, by any of the methods before-mentioned in this book, when either the Moon

or any of the Planets are on the meridian of the place the longitude is defired; for that time reduced into motion, and proper allowance being made for the difference of miles making a degree of longitude, will reduce the meridians to a true departure between the two meridians, and then the longitude may be eafily found, either by Mercator's or middle latitude failing.

EXAMPLE I.

Suppose at Petersburgh, in Russia, the Moon was taken when on the meridian, by the watch well regulated, and found it on the 6th of May, 1786, to be 6h. 20 m. and that taken from 7h. 28 m. the time the Moon passes Greenwich that day, leaves 1 h. 8 m. which being reduced into motion is 17° multiplied by 60 gives 1020, the true departure between Petersburgh and London; and if the complement of middle latitude be taken between the two places, and run down in the Tables of Difference of Latitude and Departure, the longitude in the distance column opposite the departure, (when multiplied by 10, because the numbers are too large to find by inspection) will be 1780, that divided by $60=29^{\circ}$ 30'=which is too small by 00° 49' but if a canon be stated as proper difference of latitude: the meridian difference of latitude: departure to the difference of longitude, it will come out 30 19' the true longitude required?

As proper dif. of latitude : Meridian dif. of latitude :: Departure dif. of longitude	504 899 1020	2.70243 2.95376 3.00860
	in the distance	5.96236
itudes cue tell within three in	ie ukingiba in	2.70243
True longitude from London 6(0)181	1819 (9 30° 10'	3.25993

EXAMPLE II.

June 10, 1786, suppose the Moon was taken when on the meridian of the Lizard, and found it 11 h. 25 m. 16"; now the Moon was on the meridian of Greenwich that day 11 h. 12'.

Sub. 11 12 on meridian of Lizard on meridian of Greenwich

o 13 16 after Greenwich shews my ship to the West of Greenwich, that reduced into motion gives 3° 19', which reduced into miles=199; then by the aforesaid canon the longitude=5° 14' West from Greenwich.

H

EXAMPLE

THE PROPERTY OF THE PROPERTY O

EXAMPLE III.

Suppose the Moon be taken on the meridian of Barbadoes August 7th, 1786, 14h, 26m.

Legis in Accident Appellation out adding	h.	m.	8.
viz. Barbadoes	14	26	0
Greenwich on that day is	10	18	0
	4	08	-

This reduced into motion 48° 14; this multiplied by 60' gives 2894 miles, the true departure between the Isle of Barbadoes and Greenwich, and by the canon afore-mentioned, the longitude from the Isle of Barbadoes to Greenwich is 3377 miles from the East end of the said island.

EXAMPLE IV.

The Moon was taken on the meridian of Cape St. John, in Newfoundland, September 27th, 1786, 5h. 59m. 8s.: what was the longitude of St. John from Greenwich?

Hamilton California ent.	h. 1	n.	S raggers as borell
Cape St. John's	5 5		
Greenwich	3 3	9	the Moon was on
Meridian	2 0	0	8 difference of

Time reduced into motion is 35° 2×by 60=2102 miles per canon, the difference of longitude 3332 as was required, and by this new method it will not require on e tenth part the labour of the method of finding the distance of the Moon from the Sun or a fixed star.

N. B. A person expert in taking the latitude, can tell within three minutes when any heavenly body comes to the meridian; and by allowing three minutes, the departure may be truly found between one meridian and another, when the difference in miles that make a degree of longitude are properly applied: thus, if your place be in a less latitude than Greenwich, find by inspection what miles make a degree of longitude in each latitude, and add the difference to the difference of the time when reduced into motion, and it will be the true departure; but if the place be in a greater latitude, then subtract the difference, and the departure will be the true departure between the places required.

A TABLE

THE COMPLETE GESTLYATOR

1 3/1.7 7.0

TABLE II.

OF THE DIP.

OF REFRACTION.

PERFOR in taking out to this Table for the THIS Table is calcifuled TOUR viluting time. off-band fide, with you a work oferend as your counter about you rightle fore analyst the first

enarged, (which a called (graviared shirter) houses. For estand of huma calaine had, a and as the most applied to be replaced. The soft hand, while The recognitive minutes. Never 1 of most of the never hand of the contract of the contract

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the mest even against it security to site fifth and the mesting a site fitting to be subtracted.

The mesting are in a site subtracted and the formulation are also as a formulation and the formulation are a second and the second and the second are a second are a second are a second and the second are a second as a second are a second a

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OF

REFRACTION, &c.

TABLE I.

OF REFRACTION.

OBSERVE in taking out by this Table for the Refraction, that you enter the first column on the left-band side, with your altitude observed on your quadrant, (which is called the apparent altitude) and on the next against it is the refraction required. Note. You need not be so exact as to take parts for

Note. You need not be so exact as to take parts for any half degree or degree there may remain; as near as you can find in the Table, being sufficiently exact.

TABLE II.

OF THE DIP.

THIS Table is calculated for the beight you are elevated above your vifible borizon. The column on the left hand, titled The Height of the Eye, you enter with the beight you fuppofe you are elevated, and in the next over against it is dip to be subtracted.

TABLE III.

OF TIME.

FOR reducing time and motion mutually into one another, the first column centains time, as far as 24 degrees, minutes, and seconds. The other motion, as far as 360 degrees, minutes, and seconds, answering to the first, by which any quantity of time or motion may be found.

Alt.	Ref.	Alt.	Ref.	Height of eye		Dip of boriz	Time	1	Motion
•				Feet	1	' p	H '		1
1 1 1 1 2 2 2 1 5 3 3 1 4 4 1 5 5 5 1 2 6 6 1 2	30 ¹ / ₂ 28 ¹ / ₂ 24 ¹ / ₂ 21 18 ¹ / ₂ 14 ¹ / ₂ 13 12 10 ₂ 8 ¹ / ₃ 8	7 8 9 10 11 13 15 17 19 25 32 43 62 90	7 ¹ / ₂ 6 ¹ / ₂ 5 ¹ / ₂ 5 4 3 ¹ / ₂ 2 1 ¹ / ₂ 00	1 2 5 7 10 14 18 22 28 40 50 60 80 100		1 1 1 1 2 2 2 1 2 3 3 3 4 1 2 5 6 6 7 2 7 2 8 7 3 9 1 2	1 2 3 4 5 6 7 8 9 10 11 12 13 14 16 17 18 19 20 21 22 23 24		15 30 45 60 75 105 120 135 150 165 210 225 240 285 300 315 330 345 360

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TABLES

1784, 1788, 1792, 1796, 1800.

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SUN'S DECLINATION,

M. W. M

FOR

The LEAP YEARS, &c.

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TABLE of the SUN's DECLINATION,

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For the LEAP YEARS,

1784, 1788, 1792, 1796, 1800.

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Ja	n.	F	eb.	Ma	ırch	A	pril	M	ay	Ju	ine	J	uly	Au	guit	Se	pt.	0	a.	N	ov.	D	ec
D.	М.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M	D.	M.	D.	M.	D.	M.	D.	M.	D.	M	D.	1
23			10	7	16	14	51	15					6	17	53	8	31	3	291	14	43	21	5
22	57	16	52	6	53	5	13	15			18	23			38	7	41	3	52	15	-		
22	52	16	34		30	5		15			-	253 V 4	20		22	7		4	15	15		22	1
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22	32	15	40	5	21	6	45	16	45	22	45	22	40	16	33	6	11	5	24	16	15	22	3
22			22	4	57	7			1	22	51	22	33	16	16	5	50	5	48	16	-		4
22	18	15	3	4	35	7	30	17	18	22	56	22	26	16	0	5	26	6	10	16	50	22	5
22	9	14		4	11	7	52	17	34	23		-	19	15	42	5	4	6	33	17	7	22	5
22		14	25	3	47	8			50	23	6	22	12	15	24	4	41	6	56	17	24	23	
21	15	14	5	3	23	8	36	18	5	23	10	22	3	15	6	4	18	7	19	17	40	23	
21	42	13	44	2		8					14	21		14	49		55					23	1
21	32	13				9	20	18	35	23	17	21	46	14		3		8	4	18			1
21	21	13	6	2			41	18	49	23	20	21	37	14	11	3		8	26	18			1
21	11	12	43	1	49	10	2	19	3	23	22	21	28	13	52	2	45	8	49	18	43	23	2
21	1	12	24	1	25	10	24	19	17	23	24	21	17	13	34	2	22	9	11	18	58	23	2
20	48	12	3	1	2	10					26	21			14	1	59		33	19	-		-2
20	36	11		1	38	11		19	44	23	27	20	57	12	54	1	36	9		19	- 1	23	2
20	24	11	20			11		19			28	20	46	12		1		10			41	23	2
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19	58	10	38		33	12	6	20	9	23	20	20	23	11	54		26	10	50	20	8	23	20
19			16	129	57	12	27	20					11	11	35	S.	31	1					20
19			54	1	20	12	46	20	33	23			58	II	15			1	42	20	33	23	2
19	15	9	31	1	-43	13	7	20			27	19	46	10	54		44 1	2	2'	20			2
19	2	9	8	2	7	13	26	20	55	23	25	19	33	10	331	1	8 1	2	23 2	20		23	2
18	46	8	47	2	31	13	46	21	6	23	23	19	19	10	12	1	31/1	2	44	21	8	23	2
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A TABLE of the SUN's DECLINATION,

For the First after LEAP YEAR,

1785, 1789, 1793, 1797.

		S.		S.		S.		N		N.		N.		N.		N.	a lie	N.		3.		s.	. !	3.
78	Ja	ın,	F	eb.	Ma	arch	A	pril	M	lay	Ju	ine	J	uly	Au	gust	S	ept.	0	a.	N	ov.	D	ec.
Days	D.	M.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M
1	22	59	116	54	17	22		45	15		22		23	7	17	57	8	8		23	14	37	21	5
2	22	53	16	39	6	59		8	15		22		23		17	41	7	46	3	46	14	57	22	
3	22		16	21	1 -	36		31	15		22	-	22		17	26	7	24	4	9	15		22	1
4	22		16	3	6	13	5	54	16	1.12.20	22		22	53		9	7	2	4	32	15		22	2
5	22	34	-	44	5	50	-	17	16	24	22	37	-	47	_	54	6	30	4	56	-	52	22	2
6	22		15	26	1 3	26			16	41			22		16	37	6	17	5	19	16		22	3
7	22	19	1	7		4	7	2	16	57	22		22	35		20	5	55	5	42	16	28	22	4
8	22	11	100	44		40			17	14	1	55		11000	16	3	5	32	6	5	16		22	4
9	22	2	177	. 29		17	7	47	17	30		45	22	21	1 0	45	5	9	6	28			22	5
0	21	53	14	10	3	53	8	9	17	45	23	5	22	14	15	28	4	. 46	6	50	17		23	
1	21	44	13	50	3	29	8	31	18	1	23	9	22	5	15	11	4	23	7	12	17	36	23	
2	21	34		30	3	5	8	53	18	16	1	12		5.7	14	52	4	22	7	36	17	52	23	1
3	21	33		10	2	42		15	18	31	23		21		14	34	3	37	7		18	9	23	1
14	21	24		49	2	18	1 -	36		40	23		21	40		15	3	14	8	21			23	1
15	21	13	12	28	1	55	9	57	19	11.0	23	21	21	29	13	57	2	51	8	43	18	39	23	. 2
16	20	52	12	8	1	31	10	19	19	14	23	24	21	21	13	38	2	28	9	5	18	54	23	2
7	20	35		47	1	8	10	40	19	27	23	25	21	10	13	19	2	4	9	27	19	9	23	2
8	20		11	26	1	44	11		19	40			20		13		1	41	9	49	19		23	2
9	20	14	11	4		20	103		19	53			20	49		39	1	-	10	1000	19		23	2
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21	119	48	10	21		27	12	2	20	18	23	29	20	25	11	- 59			10	5.4	20	4	23	2
22	119	33	9	59	1	51	12	23	20	30		29		14	11	39	1	-	11	15	20		23	2
23	19	20	9	37	I	14	2	42	20	41	-	28	20	1	1	20	S	16	II	36	20	28	23	2
4	119	. 4		15		38	13	3	20	52	23	27		49		58	1.2	39		21	20	42	-	2
25	18	40	8	52	2	2	13	21	21	4	23	26	19	36	10	38	1	3	12		20	53	23	2
26	18	35	8	30	2	. 52	13	41	21	13	23	24	19	23	10	17	1	26	12	. 38	21	5	23	
27	+18	19		7	2	49	14		21	24	23	20		10	9	56	1	49	12	59	21		23	2
23	118		7	45	3	12	14	20	21	33	23	18		55	9	34			13	19	21	26	23	1
29	117	47	7	1919	3	53	14	37	21	43	23	15		41	9	13	2	36	13		21	36	23	1
30	417	30	1		3	57	14	56	22	51	23	11	18	27	9	51		59	13	58		46	23	1
1	417	14	Fi .		4	27	1		22		1		18	12	8	30	l		14	19		199	23	

A TABLE of the SUN's DECLINATION,

For the Second after LEAP YEAR,

1786, 1790, 1794, 1798.

		S.		s.	. 8	3.	1	٧.		N.		N.	1	N.		N.	1	1.		s.		s.	S	
	J:	an.	F	eb.	M:	arch	A	pril	I M	lay	J	ine	Ju	ily	A	ug.	S	pt.	0	et.	N	ov.	D	ec.
-	D.	M.	D.	M.	D.	M.	D.	M	D.	M.	D.	M.	D.	M.	D	M.	D.	M.	D.	M.	D.	M.	D.	M
	23	0	17	2	17	291	4	38	15		22	6	23	8	17	59	8	14		17			21	5
l	22	25	16	44	7	6	5	- 2	15		22	14	23	4		45	7	52	3		14	-	22	-8
	22	49		26	6	43	5	24	1 2		22		22		17	30	7	29	4		15		22 .	1
	22	43		8	6	26	5	47	16		22		22	54	17	14	7	8	4		15	29		2
	22	_	15	50	5	57	6		16		22	_	22		16	58	6	45	4	50	15	47	22	2
	22	29		32	5	33	6	32		37		43	22	43	16	41	6	23	5		16	5	22	3
	22	22	15	13	5	9	6	55	16		22	49	22		16	25	6	0	5	36		23		4
	22	14	14	54	4	45	7	17.00	17		22	54	22	-	16	8	5	37	5		16	41	22	4
	22	. 5	14	35	4	23	7	40		26	5000	59	22	-	15	51	5	15	6		16	59		5
	21	50	14	15	4	C	8	2	17	41	-		22	15	15	33	4	52	-	44	17	16		59
ı	21.	47	13	56	3	36	8	24		- 57	23	8	22		15	15	4	29	7	7	17	32		
	21		13	36	3	13	8		18	12	23	12	100000	59	14	57	4	7	7	30		48		
н	21	26		15	2	48	9	10000	18	27		15			14	39	3	44	7	52			23	1
п	21	16	100000	56	2	24	9		18	0.000	23	18		41	1000	21	3	21	8	15		20	-	1
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l	23	42	0.000	53	1	15	10	33	19	24	23	- 2	21	13		24	2	11	9	21		-	23	24
l	20	30	11	32		50	11		19	37		27		-	13	5	I	48	9		19		23	20
	20		11	10			11		19	50		28				45	1	25	10	-	19	33		2
	20	- "	10	48			11	36	-	_	23	29	20	41	12	25	1	-1	10	27	19	47	23	20
	19	50	10	25	N	20	11	56			23	29	20	29		46		37	10	49		0	23	29
	19		10	5			12	16			23	- 2	20	17		40		15	11	10	0.02610	14	23	29
	19	23	9	43	1		12	36		38	-	28			11	25	S	9	II	30			23	28
	19	8	9	21	I	0	12	30	20	50	-	6	19	52		4		33	11	51		39		26
	18	53	8	58	1	54	13	16	21	1	23_	26	19	40	10	43		56	12	12	20	50	23	25
	18	38	8	30	2		13	35	21	11	33	24	19	27	10	22	1	19	12	33	21		23	23
	18	24	8	14	2		13	55	21	1000	43	21		3	10	1	1		12	201	21	13	-	21
	18	8	7	51	3	6		13		31		18	-	59	9	40	2	100	13	-	21	24	400	17
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۱	17	36		100	3	52	14	50		49	23	12	18	31	8	57	2		13	53	21	44		11
I	117	19		1	4	16		4	21	581			18	10	8	35			14	13		1	23	6

TABLE of the SUN's DECLINATION,

For the Third after LEAP YEAR,

1787, 1791, 1795, 1799.

		3.	S		S		N		N		1	1.	1	1.	N		N	1.	1	N.	5	;	S	3.
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Days.	D.	М.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M.	D.	M	D.	M
1	123	2	17	5	7	34	4	33	15	51	22		23	71	18	5	8	58	3	10		27	21	52
2	22	56	16	48	7	11	4	56	15	23	22	12		5	17	49	7	58	3	-	14	47	22	1
3	22	51		30	6	48	5	19	-	41					17	34	7	36	3		15		22	9
4	22	45		13		25	5	42	15		22	27	22	55		18	7	14	4	1/1000	15	25	22	17
_ 5	22	38	15	54	6	1	_	5	16	16	22	34	22	50	17,	2	6	52	4		15	43	22	25
6	22	31	15	36	5	38	6	28	16	33	22	40	22		16	45	6	29	5	6	16	1	22	32
7	22	24	15	17	5	15	6	50	16	50	22	46	22	38		29	6	7	5	29	16	19		39
8	22	16	14	58	4	52	7	12	17	6	22	2	22	0	16	12	5	44	5	0	16	37	22	45
9	22	7	14	39	4	28	7	35	17		22	57	22	24		55	5	21	6		16	54		51
10	21	58	14	20	4	. 5	7	57	17	38	23	2	22	17	15	37	4	58	6	38	17	11		57
11	21	49	14		3	51	8	19	17	53	23	7	22	9	15	20	4	36	7	1	17	28	23	2
12	21		13	40	3	18	8	41	18	8	23	11	22	1	15	2	4	13	7	-	17	44	23	7
13	21	29	13	20	2	54	9	3	18	23	23	14	21	53	14	43	3	50	7	46	18		23	11
14	21	18	13		2	30	9	25	18		23	18	21	44	14	25	3	27	8	9	18	16		15
15.	21	8	12	42	2	7	9	46	18	5.2	23	21	21	34	14	6	3	4	8	32	18	32	23	18
16	20	:56	12	19	1	43	10	8	19	7	23	23	21	25	13	47	2	41	8	54	18	47	23	21
17	20	.45		50	1	19	10	29		20	_	25	21	15	_	28	2	17	9		19	2	23	24
18	20		11	37		56		50		34	23	27		4	13	9	1	54	9	38	19	16	23	26
19	20		11	15					19	47		28	20	53	12	50	1	30	10		19	31	23	27
20	20	8	10	54		8	11		20		23	29	20	42	12	30	1	7	10	22	19	44	23	28
21	20	57	IC		N.	15	11	52	20	12	23	29	20	31	12	10	8.	43	10	43	19	58	23	29
22	20	44	10	10			12	12	1	24	-	29	20	20	0.5	50		20			20	11		29
23	20	33		48	I	2		32	20		23		20	8	11	30	S.	4	11	26	20	23	23	28
-24	19	13		26		26	12	52	20	47	-	28	19	56	11	10		27	11	46	20	36	23	27
25	18	58	9	4	1	50	13	12	20		23	27	19	43	10	48		51	12	7	20	47	23	26
26	18	43	8	42	2		-	31	21	_	23	25	19		10	27	1	14	12	28	20	59	23	24
27	18	27		19		37	13		21		23	-	19		10	6	1	37		48	21	70.00	23	22
28	18	12		56		0,	14		21		23	20	19	2	9	45	2	-	13		21	21	23	19
29	17	55			3	24	14		21		23	17	18	49		24	2	24	13	29	21	32	23	16
30	17	38			3				21		23	13	18	34		2	2	48	13	48	21		23	12
31	117	21			4	10			21	56			118	20	-	41			14	8			23	8

FABILE of the SUN'S DECLINATION

For the Third afterd. EAR VEAR

1787, 1791, 1795, 1799

	3.2	M		M	,VI	M	K	34.	1.2	, E		
LINE -				ANE OF S		gent.	YES	MonA	dominik			
	16.00	D. Is.	134 G	FIR . G	151. 41	14 .61	NILLS	Had of	14.2	2		ed let
			16.1 8			to to be	1 7 7		See A			
			104					DE E	THE Y			
				No. 21		22 62	42 12	月期 文				
			102 3	15 1.11		102 35		12 0	100	152 152	2454	
			TO THE			12 4				35 15	120	100
		100 1		THE REAL PROPERTY.		45	102 18		126 8			
				218 011		122 55		HEE S				
				230 271		100	92.13	图28	THE E		DOM:	1
	line in						28/83		BOY			
a water				0.5 24								TRUCK
			17 14									351.3
				4 4		lia an				PE S		基料
			100	333 ATA		23- 45			1987 F.			西川市
		The se			18	Tag Es			Beth	The cate		
		126 8	1000 5	In he								
				2 M	AG	1		0 281	161	100 11 12		
				10			44.15					100
		SER D	1 2 2 2	100		NEW TOTAL		SEE LE	77 11/4			
		125.0	U.S. de				51	The state of				
				100			10 0	2 2 2 5		131. 9		
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			Har			US WEL		See Line	Hand.			
		A STATE OF THE PARTY OF									149 TF	THE PARTY
						1627 24				THE STATE OF		
		THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TW	1	1944 0	1 63				1000.8			
			11113	140 10 1	12 145	130 80				Paul		2/11/2
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A TABLE & MARTINAS SINES IND DECANTS LESS RADIUS!

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TABLE

OF THE

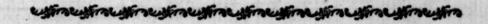
SECANTS LESS RADIUS;

OR, THE

ARITHMETICAL COMPLEMENT of the COMPLEMENT SINE,

TO

EVERY MINUTE of the QUADRANT.



A TABLE of NATURAL SINES AND SECANTS LESS RADIUS.

Zw.	D.	0.			D	. 1.			D	. 2.			
M	N. S.	S. L.R.	N. S. I	S. L. R.	N.S.	S.L.R.	N. S.	S.L.R	N. S.	S. L. R.	N. S.	S. L. R.	M
. 0	0	0.00000	00000	0.00 000	1745	0.00007	99985	1.75814	3497	0.00026	99939	15-45718	60
1 2	29			3.53627	774	,007	984	5097	519	027	938	5358	59
3	58 87	000	999	05915	803	007	984	4391 3696	548	028	937	4646	58
4	116	The second second		2.93421	862	008	983	3012	606	028	935	4295	56
_5	145		999	8 3 7 3 0	891	008	982	2339	635	029	934	3946	55
6	175		99999	2.75812	1920		99982	1.71676	3664	0.00029	99933	1.43600	54
7 8	204	000	999	63318	949	008	981	0379	693	030	932	3257 2916	53
9	262	000	999	58203	2007	000	980	69745	752	031	930	2579	51
10	291	000	999	53627	036		979	9121	781	031	929	2243	50
11	320		999	49488	065	009	979	8505	810	032	927	1911	49
12	349 378	0.00000	99999	42233	123	01000.0	99978	7298	3839	0.00032	99926	1,41581	48
14	407	000	999	39015	152	010	977	6708	897	033	924	0928	46
15	436		999	36018	181	010	976		926	034	923	0605	45
16	465	000	999	33216	211	011	976	5550 4982	953 984	034	922	0285	44
18	524	0.00001	999	30583	240	0.00011	975	1.64422	4013	0,00035	99919	39967	43
19	553	001	99999 998	25752	298	0.00011	974	3869	042	036	918	9338	42
20	582		998	23525	327	012	973	3322		036	917	9026	40
21	611	001	998	21406	356	012	972	2783	100	037	916	8718	39
23	669	COI	998	19385	385	013	972	1724	158	037	915	8411	38
24	698	0.00000	99998	2.15607	2443	0.00013	99970		4188	0.00038	99912	1.37804	36
25	727	001	997	13834	472	013	969	0690		039	911	7503	35
26	756	001	997	12130	501	014	969	0182	246	039	910	7205	34 .
27	814	100	997 997	08912	530	014	968	59680	304	040	909	6615	33
29	844	002	996	07388	589	015	966	8694	333	041	906	6322	31
30	873		99996	2.05916	2618	_	99966		4362	0.00041	99905	1.36032	30
31	902	002	996	04492	647	015	965	7728	391	042	904	5744	29
32	931	002	-996	03113	676	016	964 963			042	902	5457	28
34	989		995	0048	705	016	963			044	900	5173 4890	26
35	1018	002	995	1.99221	763	017	962	5861	507	044	898	4600	25
36	1047	0.00002	99995	1.97998	2792	0.00017	99961	1.55406	4536	0 00045	99897	1.34330	24
37 38	105			96808	821	017	960		565 594	045	896 894	4053	23
39	134	1	9 22TI		879	018	959		623	046	893	3777 3507	21
.40	164	003	993	93422	908	018	958	3634	653	047	892	3231	20
41	19:		993	92350	938	019	957	3201	682	048	890	2961	19
42	251		99993	90282	995	0.00019	99956	2350	740	0.0048	99889	2425	18
.44	:280	004	992	89283	3025	020	955 954	1931	769	049	886	2159	16
.45	309	004	991	88307	054	020	953	1515	798	050	885	1896	15
46	338	004	991	87353 86419	112	021	952	0696	827	051	883 882	1633	14
48	1396	0.00004	99990		-	0.00021	952	1.50292	4885	000052		1.31114	13
49	425	004	990	84609	170		950	49892	924	052	879	0856	11
50	454	005	989	83732	199	022	949	9496	943	053	878	(600)	10
51 52	483		989 989	82872 82029	228	023	948	9103 8713		054	876 875	0346	8
53	542		988	81202	286	023	947 946	8327	030	054	873	29841	7
54	1771	3.00005	99988		-	0.00024	99945	1.47945				1.29591	6
55	600	006	.987	79593	345	024	944	7566	088	056	870	9342	5
56	629		987 986	78811		025	943	719° 6817		057	869 867	9095	4
57	687	006	986	77287		026	942	6448		058	866	8605	3 2
59 M	716	006	985	76554	461	026	940	6081	205	059	864	8362	1
M			D.	89.			D.	88.			D.	87.	M

-	1 D	. 3.	11	3 Q /	11	D. 4.	11		I). 5.	1	National Association	
M	N. S.	S.L.R.	N. S	S.L.R.	N. 5	S.S.L.R	N. S	S.L.R.	N. 8	. S. L.R.	N S.	S.L.R.	M
0	5234	0.00060	99863	1.28120	6976	60.00100	99756	11.1564	8716	0.00166	9961	011.05970	60
1	263	60		7880							61	826	59
2	292	61		7641	06:				11 11	168			58
3	321	62		7401				492		170			57
4 5	376	63		6931	121		11 - 14	748	860	171	60		55
6	5408	0.00064	99854	1.26697	7150	0.00111	99744				9960		54
7 8	1 437	64	852	6465	175	112	742	395	918	173	60:	4971	53
	466	65	850	6233	208		740	220	11 /11	175	599	830	52
9	495	66		5774				3872	976		596		50
10	524 553	67	846	5546		1		699		177	594		49
12	5582	0.00068		1.25320			99731	1.13256		3.00179			48
13	611	68	842	5094	353			355	092	180	586	133	47
14	640	69	841	4870	382	119	II - Comment	184	121	181	583	3995	46
15	669	70		4647	411			013	150	183	580	857	45
16	698	71	838 836	4425	469		728	2844	179	184		720	44
17	727	71	99834	1.23985		0.00122	-			0.00186	575		-
18	5756 785	73	832	3766	527	123	99719		266	187	99572		42
20	814	74	831	3549		124	11			188	567	175	40
21	844	74	829	3333	585	1 125	742	005	324	190	564	040	39
22	873	75	827	3117	614	The second second		1839	353	191	562		38
23	902	76	826	2903	643	127	708	674		192	559		37
24	5931	0.00077	99824	1,22690 2478			99705	1.12510	14	0 00193	99556		36
25 26	960	77		2267	730	129	703	183	440	194	553 551	504 371	35
27	6018	79	819	2057	759		699	020	498	197	548	238	33
28	047	80	817	1848	788	132	696	0858	527	198	545	106	32
29	076	80	815	1640	817	133	694	696	1	199	. 542	1974	31
30	6105	0.00081	99813	1.21432	7840	0.00134	99692	1.10536	9585	0.00200	9954c	1.01843	30
31	134	82	812	1226	877 904	135	689	375	614	202	537	712 581	29
3 ² 33	163	83	808	0817	933	137	685		671	203	534	451	27
34	221	84	806	0614	962	138	683	09898	700	205	528	321	26
35	250	85	804	0412	991	139	680	740		207	526		25
36	6279	0.00086	99803	1.20211		0.00140	99678	1.09583	9758	0.00208	99523	1.01063	24
37	308	87	801	19811	049	141	676	426	787	209	520	0934	23
38	337 366	87	799 797	9612	107	142	673	115		210	517		22
40	395	89	795	9415	136	144		8060	874	213	511	- 550	20
41	424	90	793	9218		145	666	805	903	214	508	423	19
42	6453	0.00091	99792	1.19022	8194	0.00146	99664	1.08651	9932	0.00215	99506	1.00296	18
43	482	91	790	8827	223	147	661	498	961	217	503	170	17
44	511	92	788 786	8633 8440	252	148	659	345 193	990	218	500		16
45	540	93 94	784	8248	310	150	654	041	048	220	497	0.99918	15
47	598	95	782	8056	339	152	652	7890	077	222	491	793 668	13
48	6627	0.00096	99780	1.17866	8368	0.00153	99649	1.07759	10106	0.00223	99488	0.99544	12
49	656	96	778	7676	397	154	647	589	135	224	485	419	11
50	685	97	776	7487	425	155	644	439	164	225	482	296	10
51 52	714 743	98 99	774 772	7299	455	156	642	260	192	227	479 476	049	9
53	773	100	770	6925	513	158	637	6993	250	229	473	8926	7
54	6802		99768			0.00159		1.06846	10279	0.00231		0.98804	6
55	831	102	766	6554	571	160	632	699	308	232	467	682	5
55	860	102	764	6370	600	161	630	552	337	233	464	560	4
57	882	103	762 760	6004	629	162	627	406	366	235	461	439	3
58	918 947	104	758	5823	687	164	625	26c	395 424	236	458 455	318	2
59 M	24/	105	D.	86.			D.		1.7	-3/	D.	84.	M
717				- h	111111111111111111111111111111111111111	the state of	*		40000	1		-4.	

	D	6.			D	. 7.		9 -0	D	. 8.		C.U.	-
M	N. S.	S. L. R.	N. S.	Petrolizani di Salah		S.L.R.	N. S.	S.L.R.	N. S.	S. L. R.	N. S.	S. L. R	M
0	10453	THE RESERVE OF THE PARTY OF	99452			0.00325		0.91411	13917	0.00425	99029	0.85644	60
2	482	240	449		216	1 3	251	308	946	426	023	555	59
3	540	243	443	717	245				975		015		58
4	569	244	440	598	302		240	001	033		011	And the second	57
_5	597	245	437		331	333	237	0899	061	434	006	4	55
6	10626		99434		10360	0.00334	99233		14090		99002	0.85109	54
8	684	248	431	126	389 418		230		119		8998	020	53
. 9	713		424	008	447	337 339	222	595 494	148	439	994		52
10	742	252	421	6891	476		219	394	205	CONTRACTOR OF THE PARTY OF THE	986	755	51
11	771	253	418		504	342	215	293	234	444	982	667	49
12	10800	0.00255	99415	0.96658	12533	0.00344	99211	0.90193	14263		98978		48
14	858	256	412	542 426	562 591	345 347	208	0093	292		973	492	47
15	887	259	406	310	620	349	200	89994 894	320 349	450 452	969		46
16	916	260	401	195	649	350	197	795	378	454	961	230	45
17	945	262	399	080	678	352	193	696	407	455	957	143	43
18	10973	0.00263	99396	0.95966		0.00353	99189	0.89598	14436	0.00457	98953	0.84056	42
20	031	266	393	851 738	735	355	186	499	464	459	948	3979	41
21	050	- 267	390 386	624	793	357	178	4C1 3O3	493	461	944	884	49
22	089	269	383	510	822	360	175	205	522	465	940 936		39
23	117	270	380	397	851	362	171	107	580	467	931	626	37
24		0.00272	99377	0.95285	12880	0.00363	99167	0.89010	14608	0.00468	98927	0.83540	36
25	205	273	374	060	908	365	163	8913	637	470	923	455	35
27	234		37° 367	4948	937 966	367 368	160	816	666	472	919	369	34
28	263	277	364	836	995	370	152	719 623	695	474 476	914	284	33
29	291	279	360	725	3024	371	148	526	752	478	906	199	32
30	11320	0.00280	99357	0.94614	13053	0.00373	49144	0.88430		0.00480	98902	0.83030	30
31	349	282	354	503	081	375	141	334	810	482	897	2045	29
33	378 407	284	351 347	393 283	130	376 378	137	239	838 867	483	893		28
34	436	286	344	173	168	380	133	048	896	485 487	889 884	777 693	27
35	465	287	341	063	197	382	125	7953	925	489	880	600	26
36	Market Street, or other Parket	0.00289		0.93954	13226	0.00383	99122	0.87858	14954	0.00491	98876	0.82526	24
37	523	290	334	845	254	385	118	764	982	493	871	442	23
39	552 580	293	331	736 628	283 312	387 388	114	669	5011	495	867	359	22
40	609	295	324	519	341	390	106	575	069	597	363 858	276	21
41	638	296	320	411	370	392	102	388	097	499	854	193	19
42	1166-	0.00298	99317	0.93304	13399	0.00393	99098	0.87294		0.00503	98849	0.82027	18
. 43	696	299	314	089	427	395	094	201	155	505	845	1945	17
45	725 754	304	310	2982	485	397	091	108		506	841	863	16
46	783	304	303	876	514	399	087	6922	212	508	836 832	780	15
47	812	305	300	769	543	402	079	829	270	512	827	698	14
48	11840	3.00307		0.92663		0.00404		0.86737			- 1	0.81535	12
49	009	308	293	558	600	405	071	6451	327	516	818	453	11
50	898	311	295	452	629	407	067	553	356	518	814	372	10
52	956	313	283	347	687	411	063	370	385	520	809	291	9
53	985	314	279	137	716	412	055	278	414	522	805	129	8
5+	12014	0.00316		0.92052	13744	0.00414		0.86187		0.00526		0.81048	7
55	043	317	272	1928	773	416	047	096	500	528	791	0067	5
50	071	319	269	824	802	418	043	000	529	530	787	887	4
57	120	320	265	617	831	419	039	5915	557	532	782	807	3
59	158	323	258	514	888	423	035	738	586	534	77.8	727	2
Mil		-	1 D. 8			1	D.		013)	536	773	647	1
DESIGNATION		4	1131113		1000	10	D	82 11		1	D.	21.	M

D.	9.	14 14 E	THE PERSON	D	. 10.	12.000	Set Line	1 0	. 11,	13.53	18000	5300
				N. S	-	The second second second	THE PERSON NAMED IN COLUMN 2 I	Distance of the last	S.L. R	-	S.L.R.	M
15643	0.00538	98769	10.80567	17365	13.00665	99481	10.76033				071940	60
672	540	764	487	393			5961	109			875	59
The second second			408		672	471	810	138	812	146		58
730						460	747		815	140	681	56
			170	508					818	135	- 616	
			0.80091	17537			0.75605	19252	0.00820	98129	0.71552	54
845		737	012	565		445	534	281			488	53
873	554	732	79933	594		11		309			The second second	52
	550	728				11						50
	550	718		1 12		11			833	101	2000 2000 CM	49
		_			-					98006	-	48
	564				694		112		838	190	104	47
100	566	704	465	766		409	042	481	840		040	46
074	568	700		794			4972	509	834		Contract Con	45
103		695			A C. C. C. TONE				848		850	44
_												43
			0.79155			281	603	623	852		The state of the s	41
									855		660	40
	581		8924	966	712	373	555	680	858	044	597	39
275	583	667	847	995	715	368			860	c39	5.34	38
304			771						-			37
16333	0.00587						0.74348					36
		652	0.0 20000000000000000000000000000000000	100000000000000000000000000000000000000				822		A		35
			466				NO. 310-38-179-72231	851		The second second	221	34
	595	638		166			073		876	004	159	32
	598	633	315	195	731	331	005	908	-	7998	097	31
16505	0.00600	98629	0.78239		0.00733		0.73937			97992	0.70034	30
533	602	624	164									20
		619	PACE LAND COMP	1								28
							665		891		787	26
			863	367		299	597	079	894	963	725	25
		98600	0.77789	18395	0.00748	98294	0.73530	20108		97958	0.69664	24
706	615	595	714	424			462	136	899	952		23
734	617	590	639	452	752		395	105		946		22
	619	585	505	401			261	222			418	21
	622					267		250	909	928		19
					0.00762	98261		20279	0.00912	97922	0.69296	18
878		565	269	595	764	256	060	207	914	916	235	17
906	630	561	195	624			2993					16
935												15
												13
								-				12
	641	526	820	767	779		661	478	930	881	871	11
078	643	531	756	795	781	218	595	507	933	875	811	10
107	645	520	683	824	783	212	529	535	936	869	75C	9
136	1 647	521		852			403					
	649		537							057		7 6
17193	0.00652	98511	0.76465	18910			266	640		97851	5.00570	
	054	500						677		810		5 4
	658	406			798		136	706		833		3
208	660	401		9024	. 800	174	070	734	954	827	331	2
336	663	486	105	e52	803	168	005	763	957	821	272	1
	N. S. 15643 672 710 730 758 787 15816 845 873 902 931 959 15988 6017 056 074 103 132 16160 189 218 246 275 304 16333 361 390 419 447 476 16505 533 562 591 620 648 16677 706 734 763 792 820 16849 878 906 935 964 992 17021 050 078 107 136 164	N. S. S.L.R. 15643 0.00538 672 540 710 542 730 544 758 546 787 548 15816 0.00550 845 552 873 554 902 556 931 558 902 556 931 558 959 56c 15988 0.00562 6017 564 074 568 103 571 132 573 16160 0.00575 189 577 218 579 246 581 275 583 304 585 16333 0.00587 361 589 390 591 419 593 447 596 476 598 16505 0.00600 533 602 547 606 620 608 648 610 16677 0.00612 706 734 763 709 621 820 623 16849 0.00625 878 628 906 630 935 632 964 634 992 621 820 623 16849 0.00625 878 628 906 630 935 632 964 634 992 636 17021 0.00638 078 643 1979 621 820 623 16849 0.00652 878 628 966 630 935 632 964 634 992 621 820 623 16849 0.00652 878 628 966 630 935 632 967 636 978 643 107 645 136 647 164 649	N. S. S.L.R. N. S. 15643 0.00538 98769 672 540 764 710 542 760 730 544 755 758 546 751 787 548 746 15816 0.00550 98741 845 552 737 873 554 732 902 556 728 931 558 723 959 566 704 056 566 704 056 566 704 074 568 700 103 571 695 132 573 690 16160 0.00575 98686 189 577 676 189 577 676 189 577 676 189 577 686 189 586 662 16333 0	N. S. S.L.R. N. S. S.L.R. 15643 0.00538 98769 0.80567 672 540 764 487 710 542 760 408 730 544 755 328 758 546 751 249 787 548 746 170 15816 0.00550 98741 0.80091 845 552 732 79933 902 556 728 855 931 558 723 777 959 56c 718 698 15988 0.00562 98714 0.79620 6017 564 709 542 074 568 700 387 103 571 695 309 132 573 696 0.79155 666 704 465 001 74 568 700 387 130 578 667 <td> N. S. S.L.R. N. S. S.S. S.S. </td> <td> N. S. S. L. R. 98769 0.80567 17365 1.00665 17365 1.00665 17365 1.00665 17365 1.00665 17365 1.00665 17365 1.00665 17305 17305 1.00665 17305 17305 1.00665 17305 17537 100678 17538 100678 1006</td> <td> N. S. S.L.R. S. S. S. S. S. S. S. </td> <td> N. S. S.L.R. N. S. S.L.R. N. S. S.L.R. S. S.L.R. S. S.L.R. S. S.L.R. S. S.L.R. S. S.L.R. S. S. S.L.R. S. S. S.L.R. S. S. S. S. S. S. S. </td> <td> N. S. S.L.R. S. S. S. S. S. S. S. </td> <td> N. S. S.L.R. N. S. S.L.R. N. S. S.L.R. N. S. S.L.R. S.L.R. </td> <td> N. S. S.L.R. N. S</td> <td> N. S. S.L.R. N. S</td>	N. S. S.L.R. N. S. S.S. S.S.	N. S. S. L. R. 98769 0.80567 17365 1.00665 17365 1.00665 17365 1.00665 17365 1.00665 17365 1.00665 17365 1.00665 17305 17305 1.00665 17305 17305 1.00665 17305 17537 100678 17538 100678 1006	N. S. S.L.R. S. S. S. S. S. S. S.	N. S. S.L.R. N. S. S.L.R. N. S. S.L.R. S. S.L.R. S. S.L.R. S. S.L.R. S. S.L.R. S. S.L.R. S. S. S.L.R. S. S. S.L.R. S. S. S. S. S. S. S.	N. S. S.L.R. S. S. S. S. S. S. S.	N. S. S.L.R. N. S. S.L.R. N. S. S.L.R. N. S. S.L.R. S.L.R.	N. S. S.L.R. N. S	N. S. S.L.R. N. S

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		S. C. Addition	12.				13.	NO	S.L.R.		S.L.R	N. S.	S. L. R.	M
	M	N. S.	S. L.R.	Bed Billion	S. L.R.	-	S.L.R.	And the second second	Annual Contract of Street, or other party of the Contract of t		1		0.61632	60
	0	820	962	809	0.68212	523	131	97437	737	24192	313	97030	582	59
	2	848	965	803	093	552	133	424	682	249	316	015	531	\$8
	3	877	968	797	034	580	136	417	627	277	319	008	481	57
	4	905	970	700	7975	608	139		573	305	322	6994	380	56
	5	933	973	784	0.67857	22665	142	404	0.64464	24361	325 0.01329	96987	0.61330	55
	6	20962	0.00976 978	97778	798	693	148	97398 391	410	390	332	980	279	54
	7 8	1019	981	766	739	722	151	384	350	418	335	973	229	52
	9	047	984	760	681	750	154		302	446	338	966	179	51
	10	076	987	754	563	778	157	371	194	474	341	959	079	50
	11	104	989		0.67505	22835	0.01163	97358	0.64140	24531	0.01348	96945	0.61020	49
* .	12	161	995	735	446	863	166	351	086	559	351	937	0979	47
	14	189	998		388	892	169	345	032	587	354	930	929	46
	15	218	1000		330	920	172	338	3978	615	357	923	879	45
	16	216	003	717	272	948	175	331	9 ² 5 871	644	360	916	830 780	44
	17	21303	2.01000		0.67156		0.01181	97318	0.63818		0.01367	96902	0.60730	42
	19	331	041	97705	098	033	184	311	764	728	379	894	681	41
	20	360	014	692	040	-062	187	304	711	756	373	887	631	40
	21	388	017	686	6982		190		658		377	880	582	39
	22	417	020	680	925	118	193		551	841	383	866	533 483	38
	23	21474	0.01025	97667	0.66810	23175	0.01199	97278	0.63498	24869	0.01386	96858	0.60434	36
	24	502	028	661	752	203	202	271	445	897	390	851	385	35
	26	530	031	655	695		205	264	392	925	393	844	336	34
	27	559	035		638	288	208	257	340	953	396	837	287	33
	28	587	036		523		211	251	234	5010	399	822	189	31
	29	21644	0.01042	-	0.66466	-	0.01217	97237	0.63181	25038	0.01406		0.60140	30
	30	672	045		409		220		129	066	409	1807	091	29
	32	701	047	617	353		223	11	076		412	1800	042	28
	33	729	050		296		226		2972	151	416	793 786	59994 945	26
	34	758	053		182		232	203	919		422	778	897	25
	36	21814	3.01059		0.66126	-	0.01235	97196	0.62867	25207	0.01426		0.59848	24
	37	843	062	585	069	542	238	189	815	235	429	764	800	23
	38	871	064		013	571	241	182	763	263	434	756	751	122
	39	928	067		5957		244		659	320	435	749	703 654	21
i.s.	40	956	073		844		250	11	607	348	447	734	606	119
	42	21985	5. 10076		0.65788	23683	0.01254	97155	0.62555	25376	0.01445	96727	0.59558	18
	43	2013	079	547	732	712	257	148	50	404	439	719	510	:17
	44	041	081	11 .	676	740	260		451	432	452	712	462	116
	45	070	084	534	564		265		348	460	455 459	697	414 366	15
	47	125	691	1	509	825	267	120	297	516	462	690	318	13
	48	22155	0.01093	97515	5.65453	23853	0.01272	197113	0.62245	25545	0.01465	96682	0.59270	12
	49	183	096	0 508	398	882	275	106	194	573	469	675	222	CII .
	50	212	,099	502	342	910	278		142	601	473	667	175	10 .
	51	240	102	496	231	938	- 285	086	040	629	475	653	079	8
1	53	297	107	483	176		288	097	1989	685	482	645	032	7
	5+	22325	0.01110		0.6512	24023	0.01291	97072	0.61938	25713	0.01485	96638	3.58984	6
	50	354	112	470	066	051	294	965	887	741	489		937	-5
	50	382.	116	1 , 3	49;6	108	297	058	836	769	493	623	889 842	4
	57 58	438	119		901	136	300	051	734	826	499	608	795	3
	50	407	125	444	846	164	336	037	683	854	502	600	748	1
200	59 M			·D.	77.	1		D.	76.			D.		M

100	D	. 15.		or Ca	11). 16.			I). 17.			1
M		S. L. R.	N.S.	S. L. R.	N. S.	S.L.R.	N. S.	S.L.R	N. S.	S. L. R.	N. S.	S. L. R.	N
0	25882	10.01506	96593	0.5870	127564	,0.C1710	16126	10.5596	29237	0.01940	195630	10.53406	16
1	910	509	585	653		719	118	92:	265	94	622	365	5
2	938	512			1 1 0	72				948	11 /	323	
3	966	516				727	11			953		283	
4	994	519		465		734				956		242	5
_5	6022	523				_					1	200	5
6	26050	0.01526	96547	0.58418		0.01738			29404	0.0196		0.53159	5
7 8	107	529			11 0	745	11	61	460	971		077	5
9	135			278		749	11			975	11	036	5
18	163	540		232	11 0	75				979		2995	5
11	191	543	H With Land	185		750	037	484		983		955	4
12	26219	0.01547	96502	0.58139	27899	0.0176	96029	0.5544	29571	0.01987	95528	0.52914	4
13	247	550	494	092		76	021	398	599	991		873	4
14	275	553	486	046	955	76			626	995	511	832	4
15	303	557	479	7999		77				999	502	790	4
16	331	560	471	953		774			11	2003	11	751	4
17	359	564	462	907		778				007	485	710	4
18	26387	0.01567	96456	0.57860		0.0178	59981	0.55181	29737	0.02011	95476	0.52670	4
19	415	571	448	814		78			765	014	467	625	4
20	443	574	440	768	11	789				018	11	589	4
21	471	578	433	676		793			11 0	022	11	548	3
22	500	581	417	630		800			876	030	11	467	3
-				-	11	0.01804	-	-		_			3
24	26556	0.01588	96410	539	262	808		0.54923		0.02035	95424	387	3
26	612	59: 595	394	493	11	811	915			038	11	346	3.
27	640	598	386	447	11 0	816		794	-0-	046	11	306	3
28	668	602	379	401		819	898	751	30015	050	11 0	266	3
29	696	605	371	356	374	823		708	043	054	380	226	31
30	26724	0.01609	96363	0.57310		0.01826	95882	0.54666	30071	0.02058	95372	0.52186	30
31	752	612	355	265	429	83	874	623	098	- 062	363	146	29
32	780	616		219		834		581	126	066	354	106	28
33	808	619	340	174	11	838		538		070		066	27
34	836	623		083	1 2 3	841	849	496		074	337	026	26
35	864	627	324		541	845	841	453	209	078	328	1986	25
36	26892	0.01630	90310	0.57038	28569	0.01849	95832	0.54411	30237	0.02082	95319	0.51946	24
37	920	634	308	6992	597 625	853	824 816	368	265	086	310	906 867	23
38	948 976	637	301 293	947	652	856 860		326	320	090	301	827	21
39	7004	644	285	857	680	864	799	241	348	098	284	787	20
41	032	648	277	817	708	868	791	196		102	275	748	19
42	27060		96269	5.56767	28736	0.01871	95782	0.54157	30403			0.51708	18
43	088	655	261	722	764	875	774	115		110	257	668	17
44	116	658	253	677	792	879	765	073	459	. 114	248	629	16
45	144	662	246	633	820	883	757	931	486	118	240	589	15
46	172	666	238	588	848	887	746	3989	514	122	231	550	14
47	200	669	230	543	875	890	740	947	542	126	222	510	13
48	27228		96222		28903	0.01894	95732	0.53905				0 51471	12
49	256	676	214	454	931	898	724	863	597	134	204	432	11
50	284	680	206	409		902	715	822	625	139	195	393	10
51	31.2	683	198	365	987	906	707	780	653	143	186	353	9
52	340 368	687	190	320	9015	910	698 690	738	68o 708	147	168	314	
53						913		697		151		275	7
54				5.56231	29070	0.01917	95681	0.53655	30736	0.02155		0.51236	6
55	424	698	166	187	126	921	674	614	763	159	151	197	5
56	452	701	158	134	154	925	656	572	791	167	133	119	4
57	508	705	150	099	182	929	647	531 489	846	171	124	080	3 2
59	536	712	134	010	209	936	639	448	874	175	115	041	ī
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	D	. 18,			D	. 19.	1	Hade	D	. 20.	1	D. 11	
M	N. S.	S.L.R.	N. S.	S.L.R.	N. S.	S.L.R.	N. S	. S.L.R.	N. S	S.L. R.	N S.	S.L.R.	M
0	30902	0.02179	195106	0.51002		0.0243	194552	10.48736	134202	0.02701	193969	0 46595	160
1	929	18:	097	0963		437	542	699		700	959	560	59
2	1 231	188		924	612	442		663		711	11	525	58
3 4	985	192		847		446		5.89		719	11	491	57
5	040	200	11 1	808		455		553	339	724	11	422	56
6	31068	0.02204	95052	0.50769		0.02459		0.48;16	34366	0.02729		0.46387	
7	095	208		731	749	464	485	480	393	734	11 (2	353	54
8	123	212	11	692		468		443	421	738	889	318	52
9	151	210	11	653	804	472		406		743		284	51
10	178	221	015	576		477		371	475	748		249	50
	-	-			-	0.02485	11-	334		752		215	49
13	31233	233	94997 988	0.50538	914	49	94438	262		762	93 ⁸ 49 839	0.46181	48
14	289	237	979	461	942	494	418	226	11 231	766		147	47
15	316	241	970	423	969	499		189	11 7 1	771	11	078	45
16	344	246	961	385	997	503	399	153		776	809	043	44
17	372	250	952	346	3024	508		117	666	780		009	43
18	31399	0.02254	94943	0.50308	33051	0.02512	94380	0.48081	34694	0.02785	93789	0.45975	42
19	427	258	933	270	079	516		045	721	790	779	941	41
20	454	262	924	232	100	521	361	009		794		907	40
21	482	266	915	194	134	525 530	351	7973	775	799 804		873	39
23	537	275	897	118	189	534	332	937	833	858		839	38
24	31565	0.02279	94888	0.50080	33216	0 02539	94322	0.47865	34857	0.02813	93728	-	37
25	593	283	878	042	244	543	313	821	884	818	718	737	36
26	620	287	869	004	271	547	303	798		822		703	35
27	648	292	860	49966	298	552	293	758	939	827	698	669	33
28	675	296	851	928	326	556	284	736	966	832		635	32
29	703	300	842	890	353	561	274	686	993	837	677	601	31
30	31730	0.02304	94832	0.49852	33381	0.02565	94264	0.47650	35021	2.02841	93667	0,45567	30
31	758	309	823	815	408	570	254	615	048	846		534	29
32	786	313	814	777	436	574 579	245	579	075	851	647	500	28
33	813	317	795	739 702	490	583	235	544 508	130	855	637	466	27
35	868	326	786	664	518	588	215	473	157	865	616	433 395	25
36	31896	5.02330	94777	0.49626	33545	0.02592	94206	0.47437	35184	0.02870	93606	0.45365	24
37	923	334	768	589	573	597	196	402	211	874	506	332	23
38	951	338	.758	551	600	601	186	366	239 266	879 884	585	298	22
39	979	343	749	514	627	606	176	331	266	884		265	21
40	2006	347	740	477	655	610		295	293	889	, ,	231	20
41	034	351	730	439	682		157	260	320	893	555	198	19
			94721			0.02619 624		0.47225	35347	0.02898		0 45 164	18
43	089	360 364	712	365 327	737 764	628	137	189 154	375 402	903	534	131	17
45	144	368	693	290	792	6331	118	119	439	913	524	097	15
46	171	372	684	253	819	637	108	084	456	917	503	031	14
47	199	377	674	216	846	642	098	049	483	922	493	4997	13
	32227	0.02381	94665	0.49179	33874	0.02647	94088	0.47014	35511			0.44964	12
49	254	385	656	142	901	651	078	6979	538	932	472	931	11
50	282	390	646	104	929	656	068	994	565	937	462	898	10
51	309	394	637	067	956	665	058	908	592	941	452	864	.9
52	337	398	628	8993	983	669	049	874	619	946	441	831	
53	364	4°3		0993	4011		039	839	647	951	431	798	7
					34038	5.02674 678	019	0.46804	35674	0.02956	93420	0.44765	6
55	419	411	599	92c 883	093	683	009	769 734	701	961	410	73 ² 699	5
57	474	420	580	846	120	688	3999	699	755	970	389	656	4 3
58	502	424	571	809	147	692	989	664	782	975	379	633	2
59 M	529	429	561	773	175	697	979	630	810	980	368	600	I
-	-		D.	71.			D. 7				D.	69.	M

	D.	21.			D	. 22.			D	3			
M	N. S.	S. L.R.	N.S.	S. L. R.	N. S.		N. S.	S. L. R	N. S.	S. L. R.	N. S.	S. L. R.	M
0	35837	0.02985	93358	0.44507	37461	0.03283		0.42642			192050	0.40812	60
1	864	990	348	544	488	289	1	611	099	603	039	782	59
2	891	995	338	501	515	294	697	580	I Committee of the comm	613	028	753	58
3	918	999	327	468	542	304		549 518	180	619		724 693	57
4	945	3004	316	436	595	309	664	486	207	624	1994	664	
5_	073				37622	_	92653			0.03630		0.40634	55
6	36000	0.03014	93293	0.44370	649	319	642	0.42455	39234	635		604	54
7 8	027	019	274	337	676	324		424 393	287	640	971 959		53
9	018	029	264	272	703	330		362		646		575 545	52
10	108	034	253	239	730	335		331	341	651	936	516	50
11	135	038	243	207	757	340		300	367	657	925	486	49
12	36162	0.03043	93232	0.44174	37784	0.03345	92585	3.42269	39394	0.03662	91914	0.40457	48
13	190	048	222	142	811	350	1 2	238	421	667	902	437	47
14	217	053	211	100	838	355	565	207	448	673	891	398	46
15	244	058		077	865	360	554	1.76		678	879	368	45
16	271	063		044	892	366	543	145	501	684	868	339	44
17	298	068	180	012	919	371	532	115	528	689	856	310	43
18	36325	0 03073	93169	0.43979	37946	0.03376	92521	0.42084	39555	0.03695	91845	0.40280	42
19	352	078	159	947	973	381	510	053	581	700	833	251	41
20	3.79	083	184	915	999.	386	499	022	608	706	822	222	40
21	406	088	137	882	8026	392		1992	635	711	810	192	39
22	434	093	127	850	053	397	477	961	661	716	799	163	38
23	461	007	116	818	080	402	466	930	688	722	787	134	37
24	36488	0.03102	93196	0.43785	38107	0.03407	92455	0.41899	39715	0.03727	91775	2 40105	36
25	515	107	095	753	134	412	444	869	741	733	764	076	35
26	542	112	084	721	161	418		838	768	73.8	75.2	046	34
27	569	117	074	689	188	423	421	808	795	744	741	017	33
28	596	122	063	657	215	428		777	822	749	729	39988	32
29	623	127	052	623	241	433	399	747	848	755	718	959	31
30	36650	0.03132	92042	0.43592	38268	0.03438	92388	0.41716	39875	0.0376	91706	0.39930	30
31	677	137	031	560	295	444	377	686	902	766	694	901	29
32	704	142	020	528	322	449	366	655	928	771	68;	872	28
33	731	147	010	496	349	454	355	624	955	777	071	843	27
34	.751	152	2999	464	376	459	343	594	40008	782 788	660	814 785	26
35	785	157	938	432	403	465	332	-	-		648		25
36	36812	0.03162	92978	0.43401	38430	0.03470	92321	0.41533	40035	0.03793	91636	0.39756	24
37	839	176	967	369	456	475	209	503	062	799 804	625	727	23
38	867	172	956	337	510	480 486	287	473 443	1	810	601	669	22
39 40	894 921	177	945	305 273	537	491	276	412		815	569	641	21
41	948	187		241	564	496	265	382	168	821	578	612	19
_			_	0.43210	28501	-	92254			0.03826	91566		18
42	36975		92913	178	617	0.03502	2:43	0.41352	226	832		3.39583	
43	7002	197	892	146	644	507 527	231	291	248	838	555 543	554 526	17
45	056	207	881	114	671	517	220	261	275	843	531	497	15
46	083	212	870	083	698	523	209	231	301	849	519	468	14
47	110	217	859	051	725	528	198	201	328	854	508	439	13
48	37134	0.03222	92849	0.43020		0.03533	92186	0.41171	40355		91496	0.39411	12
49	164	228	838	2988	778	539	175	141	381	865	484	382	11
50	191	233	827	956		544	164	111	408	871	472	354	10
51	218	238	816	225	832	549		081	434	877	461	325	
52	245	243	805	. 89;	859	555	141	051	461	882	449	296	9
53	272	248	794	862	886	560	130	021	488	888	437	269	7_
54	37299		92784	0.42831	38912	0.03566		0.40991		0.03893	91425	3.39239	6
55	326	258	773	799	939	571	107	961	541	899	414	211	5
56	353	263	762	768	966	576	096	931	567	905	402	182	4
57	380	268	751	. 736	993	581	085	902	594	910	390	154	3
58	407	273	740	705	9020	587	073	872	621	916	378	129	2
59 M	434	278	729	674	046	592	062	842	647	921	366	097	1
	-	-		68.			1)	67.				66.	M

	D	. 24.			D	25.			D,	26.	Prays	THE PARTY	
M	N. S.	Designation of the last of the		S.L.R.	Contract of the Contract of th	S.L.R.		S.L.R.	11	S.L.R.		S.L.R.	M
0		0.03927	91355	10.39069	142262	10.04272		0.37405	43837	0.04634	89879	0.35816	
1	700	933	343	040	288	278	618	378	863	640	867	790	59
2	727	938	331	8984	315	284	594	351 324	889	646		764	58
3 4	753	945	319	955	341	296		297	942	659		712	57
5	806	955	295	927	394	302	569	270	968	665	816	687	55
6	40833	0.03961	21283	0.38895	12420	0.04308	90557	0.37243	43994	0.04671	89803	0.35661	54
7 8	865	960	272	871	446	314	545	216	4320	677	790	635	53
	885	972	260	842	473	320	532	189	046	68.2	777	609	52
9	913	978	248	814	499	326		162	072	69	764	583	51
10	939	983	236	786	525	332	507	135	098	696	752	557	50
11	956		224	758	552	337	495	198		702	739	532	49
12	40992	4000	91212	0.38730	42578 604	0.04343	90483	0.37082	44151	0.04708	89726	0.35506	48
13	1019	006	188	702 674	631	349 355	470 458	005	177	714	713	455	47
15	045	012	176	646	657	361	446	001	229	727	687	429	45
16	098	018	164	618	683	367	433	6974	255	733	674	404	44
17	125	023	152	589	709	373	421	948	281	739	662	378	43
18	41151	0.04029	91140	0 38562	42736	0.04379	90408	0.36921	44307	0.04746	89649	0.35353	42
19	178	035	128	534	762	385	396	894	333	752	636	327	41
20	204	040	116	506	788	391	383	867	359	758	623	302	40
21	231	046	104	478	815	497	371	841	385	764	610	276	39
22	257	052	092	450	841 867	403	358	814	411	771	597	251	38
2.3	284	058		422		409	346	787	437	777	584	225	37
24	41310	069	91068	0.38394	12894	2.04413	90334	0 36761	44464	3.04783	8957	0.35200	36
25	337	075	044	366 338	920	421	321	734	490 516	789	558	174	35
27	363	080	032	311	972	433	309 296	708 681	542	796	545	149	34
28	399	086	030	283	999	439	1 0	655	568	808	5.19	098	32
29	443	092	008	255	3025	445	271	628	594	815	506	073	31
30	11469	0.04098	90996	0.38227	43051	0.04451	90259	0.36602	44620	0.04821	89493	0.35047	30
31	496	1.3	984	200	077	457	246	575	646	827	480	022	29
32	522	109	972	172	104	463	233	549	672	833	467	4997	28
33	549	115	960	144	130	469		522	698	840		971	27
34	575	121	948	089	156	475	208	497	724	846	441	946	26
35	602	127	936	-		481	196	469	750	852	428	921	25
36	11628	0.04132	90924	0.38061	43209	0.04487	90183	0.36443	44776	0.04859	89415	0.34896	24
37 38	655	138	800	034	235	493	171	417	802	865 871	402	870	23
39	681	144	00	7979	287	506	146	390 364		878	389 376	845 820	21
40	707	156	875	951	313	512		338	880	884	363	795	20
41	760	161	863	924	340	518	120	311	906	89	350	770	19
42	11787	0.04167	90851	0.37896	43366	0.04524	90108	0.36285	44932	0.04897	89337	0.34745	18
43	813	173	839	869	392	530	095	259	958	903	324	719	17
44	840	179	826	841	418	536	082	233	984	910	311	694	16
45	869	185	814	814	445	542	070	206	5010	916	298	669	15
46	892	190	780	786	471	548	057	180	039	922	285	644	14
47	919	196		759	497	554	045	154	062	929	272	619	13
	11945	208	90778 766	0.37732	43523	0.04560 566		0.36128	45088	0.04935	89259	0.34594	12
49	972	214	753	704 677	549 575	573	019	076	114	941	245	569	11
51	2024	220	741	650	602	579	89994	350	140	948 954	232	544 519	10
52	051	225	729	623	628	585	981	024	192	961	206	494	9
53	077	231	717	595	645	591	968	5998	218	967	193	469	7
54	42104	0.04237	90704	0.37568		0.04597	-	0.53972	45243	0.04973	89180	0.34444	6
55	130	243	692	541	706	603	943	946	269	980	167	420	5
56	156	249	685	514	733	609	930	920;	295	986	153	395	4
57	183	255	668	487	759	616	918	894	321	993	140	370	3
58 59 M	209	261	655	459	785	622	905	868	347	999	127	345	2
50	235	267	643	432	811	628	892	842	373	5005	114	320	1

	D	. 27.	1		D	. 28.	2.18	edra s	D	. 29.		d ,	
M	N. S.	S.L.R.	N. S	S.L.R.	N. S.	S L.R.	N. S	S.L.R.	N. S	S.L. R.	N S.	S.L.R.	N
0	45399	10.05012	89101		146947	0.05407		13.32839		10.05818	87462	0.31443	6
1	425	018	087	271	973	413	11	815	506	825	448	420	1 0
2	451	025		246		420	III	793	532	833	438	397	5
3	477	031	061	221	7024	427		768	1 22.	839	420	375	5
4	503	038	035	296 172	050	433		744	11 -	846		352	
5	529	044	-	-	-	440	-					-	-
6	45554	0.05051	89021	0.34147	17101	0.05447	199	0.32697	48634	0.05860	87377	284	-
7 8	580	057	8995	098	127	454		650		874	363	261	5.
9	632	070	981	073	178	467	172	626		881	349	238	5
10	658	077	968	048	204	474	11 0	602		888		216	100
11	684	083	995	024	229	481		679	761	895	306	193	4
12	45710	0.05089	88942	0.33999	47255	0.05487		0.43555	48786	0.05902	87292	0.31170	4
13	736	096	928	975	281	494	177	532	811	910	11	148	4
14	762	102	915	950	306	501	103	508	837	917	263	125	40
15	787	100	902	925	332	508		465	862	924	250	103	4
16	813	115	888	901		515		461	887	931	235	080	4
17	839	122	875	876	383	521	062	438	913	938	221	058	4
18	45865	0.05129	88862	0.33852	47499	0.05528	88048	0.32414	48938	0.05945	87207	0.31035	4:
19	891	135	848	827	434	535	034	391	964	952	1	013	4
20	917	142	835	803	460	542	028	367	989	959		0990	46
21	942	148	822	779	486	549	006	344	9014	966	164	968	3
22	978	155	808	754	511	555	7993	320	440	973	150	945	3
23	964	161	795	730		562		297	065	.980	136	923	37
24	46020	0.05168	88782	9.33705	47562	0.05569		0.32274	49090	0.05988	87121	0.30900	30
25	046	174	768	681	588	570	951	250	116	995	107	878	35
26	072	181	755	657	614	583		227	141	6002	093	856	34
27	097	187	741	632	639	590	923	180	166	009	079	833	33
28	123	19+	728	6.8	665	596 603	909 896	157	192	016	063	811	32
29	149	201	715	5 34	-		1		217	023	050	788	31
30	46175	0.05207	88701	335 9	47716	0.05610		0.32134	49242	0.06030	87036	0.30766	30
31	20,	214	688	535	741	624	868	087	268	037	e21	744	29
32	226	220	661	487	767	631	854 840	c64	293 318	045	6007	721	28
33	252	227	647	463	793	638		041	344	052	6993 978	699	27
34		233	634	438	844	645	812	018	369	066	964	655	
35	304	-	88602	-		0.05651		0.31994		0.06073			25
36	46330	0.05247	607	0.33414	895	658	87798 784	971	49394	08	86949	0.30632	24
37	355	253	593	39° 366	920	665	770	. 948	445	088	935	588	23
38	407	266	580	342	946	672		925	470	095	906	566	21
19	433	273	566	318	971	679	743	902		102	892	544	20
11	458	280	553	294	997	686	729	879	522	109	878	521	19
	46484	0.05286	88539	0.33269		0.05693	87715	0.31856	49546	0.06110	86863	0.30499	18
12	510	293	526	245	048	700	701	833	571	124	849	477	17
13	536	300	512	221	073	707	687	810	596	131	834	455	16
15	561	306	499	197	099	714	673	787	622	138	820	433	15
6	587	313	485	173	124	721	659	763	647	145	805	411	14
17	613	320	472	149	150	727	645	740	672	153	791	398	13
19	46639	0.05326	88458		48175	0 05734	87631	0.31717	49697	0.06160	86777	0.30367	12
19	664	333	445	101	201	741	.617	695	723	167	762	345	11
0	690	340	431	058	226	748	603	672	748	174	748	323	10
1	716	346	407	074	252	755	589	649	773	131	733	301	9
2	742	353	404	030	277	762		626	798	189	719	279	8
3	767	360	390	006	303	769	560	603	824	196	704	257	7
4	46793	0.05366	88377	0.32982		0.05776	87546	0.31580	49849	0.06203	86690	0.30235	6
5	819	373	363	958	354	783	532	557	874	211	675	213	5
6	844	380	349	934	379	790	518	534	899	218	661	191	4
7	870	386	336	910	405	797	504	511	924	225	646	169	3
8	896	393	332	887	430	804	490	488	950	232	632	147	2
9	921	400	308	863	456	811	476	466	975	240	617	125	1
-	100000000000000000000000000000000000000	1	D.	62		*1	D.	61.			D. (10	M

	1	D. 30.	1		1). 31.	1		1). 32.	1		
M	N S	. S.L.R.	N. S	S.L.R.	N. S	. S.L.R.	N.	S.S L.R.	N. 8	5. S. L. R	N S	. S.L.R.	M
0	THE P. RESIDENCE OF	0.0624	7 86603	0.3010	151504	0.0669	3 85717	0.28816	52992	10.07158	184805		60
1		25.	4 588	081	1 0 /	76	702	79	53017	166	789	559	59
3	30		11 3/3			700		1 "		174			58
4	IN COLUMN SOL		311			72	11 -			182	1	519	57
5						73				190		478	55
6	50151	0.0629				0.06739				0.07205		0.27458	54
. 7	176		501	950	678	747		669	165	213	697	438	53
8	201	1 3 3		928	703	754	597	648	189	221	681	418	52
9	227			907	728	762	11 -			229		398	51
11	252	320	11	895	753 778	777		586		237	635	378 357	50
12	50302			0.29841		0.06785	85536	0.28565		245	84619	0.27337	49
13	327	342		820		793		544		0.07253	604	317	47
14	352	350	11	798	852	800		523		269	588	297	46
15	377	357	384	776	877	808	491	502	361	277	573	277	45
16	403	364		755		816		481		285	557	257	44
17	428	372	354	733	927	823	461	461	411	293	542	237	43
18	5°453 478	0.06379	86340	0.29712		0.06831	85446	0.28440	53435	0.07301	84526	0.27217	42
19	503	394		690		839	431	398		309	495	197	41
21	528	401	295	647	026	854	401	378	509	317	480	157	40 39
22	553	409	281	625	051	862	385	367	534	333	464	137	38
23	578	416	266	604	076	869	370	336	558	341	448	117	37
24	50103	0.06423	86251	0.29582	52101	0.06877	85355	0.28315	43583	0.07349	84433	0.27098	36
25	628	431	237	561	126	885		295	607	357	417	078	35
26	654	438	222	539	151	892	325	274	632	365	402	058	34
27	704	446		518 496	175	900		253	656	373	386	038	33
29	729	461	178	475	225	916		233	705	389	370 355	26998	32
30	50754	0.06468	86163	0.50423	52259	0.06923		0.28191	73730	0.07397	84339	0.26978	-
31	779	475	148	432	275	931	249	171	754	405	324	959	30
32	804	483	133	410		939	234	160	779	413	308	939	28
33	829	490	119	389	324	947	218	130	804	421	292	819	27
34	854	498	104	367	349	954	203	109	828	429	277	899	26
35		505		346	374	962		089	853	437	261	879	25
36	929	0.06513	86074	0.29325	52399	0.06970	85173	0.26068	53877	0.07445	84245	0.26860	24
37 38	954	520 528	045	303	423	• 978 986	157	048	902	454 462	230	840	23
39	979	535	030	261	473	993	127	006	950	470	198	800	22
40	1004	5.43	015	239	598	7001	112	27986	975	478	182	781	20
41	029	550		218	522	009	096	966	54000	486	167	761	19
42	51054	0.06558	85985	0.29197	52547	0.07017	85081	0.27945	54024	0.07494	84151	0.26741	18
43	979	565	970	176	572	024	066	925	049	502	135	722	17
44	104	573 580	956	154	597 621	032	051	904 884		510	120	702 682	16
46	154	588	926	133	646	048	020	863	097	518 527	088	663	15
47	179	595	911	091	671	056	005	843	146	535	072		13
	51204	0.06603	85896			0.07064	84989	0.27823			84057	0.26623	12
49	229	610	881	048	728	071	974	802	195	551;	041	604	11
50	254	618	866	027	745	079	959	782	220	559	025	584	10
51	279	625	851	006	770	087	943	762	244	567	009	565	9
52	304	633	836	8985 964	794	103	928	741	269	575	83994	545	
- Inches			-				913	721	293	583	987	526	7
54	51354 379	656	792	0.28942	869	119	34897 882	680	342	0.07592	83962 946	3.26506 487	6
56	404	663	777	900	893	126	866	660	366	608	930	467	5
57	429	671	762	879	918	134	851	640	391	616	915	448	3
50 1	454	678	747	858	943	142	836	619	415	624	899	428	2
59	479	686	732 1	837	967	150	820	599	439	633	883	409	1
M	Hart of	8 . C		D. 59.		THE THE	H. Carlotte	D. 58.		ALG	D. 5	7.	M

		. 33	1	3 2 1 4		. 34.			D). 35.		7 70 7	
M	N.S.	S. L. R.	N.S.	S. L. R		S.L.R.	N. S.	S.L.R.	N. S.	S. L. R.	N. S.	S. L. R.	M
0	154464	10.07641	83867	0.26389	55919	0.08143	82924	0.25244	57358	0.08664	81915	0.24141	160
L	488	649	851	370		151	887	225	381	672		123	59
2	513	657	835	350	968	160	871	206		681		105	58
3	537	665	820 804	331	56016	168		188	4	690		087	57
5	561	682	788	292	040	177		169		708	848	069	56
6	54610	0.07690	83772	0.26273	56064	0.08194	82806			0.08717	81815	051	55
7	635	698	756	253	088	202	790	0.25132		726	798	0.24033	54
8	659	707	740	234	112	211	773	094		734	781	23997	53
9	683	715	724	215	136	219		072		743	765	979	51
10	708	723	708	195	160	228	741	c56		752	748	961	50
11	732	731	692	176	184	237	724	039		761	731	943	49
12	54756	0.07740	83676	0.26157	56208	0.08245	82708	0.25020	57643	0.08770	81714	0.23925	48
13	781	748	660	137	232	254	692	100	667	779	698	907	47
14	805	756	645	118	256	262	675	4983	691	788	680	889	46
15	829	765	629	099	280	271	659	964		797	664	871	45
17	854 878	773 781	597	079	305	280 288	643	946	738 762	806	647	854	44
18					329			927		815	631	836	43
19	54902		83581 565	0.26041	56353	0.08297	82610	0.24909	57786	0.08824	81614	0.23818	42
20	927	798 806	549	002	377	305	593	890 872	809	833	597	800	41
21	951	814	533	5983	425	314 323		853	857	842 850	563	782 764	40
22	999	823	517	964	449	331	544	835	881	859	546		39
23	5024	831	501	945	473	340	11	816		868	530	747	37
24	55048	0.07830	83485	0.25926	56497	0.08349		0.24798	57928	0.08877	81513.	0.23711	36
	072	848	469	907	521	357	495.	779		886	496	693	35
25	097	856	453	887	545	366	478	761	976	895	479	676	34
27	121	864	437	868	569	375	462	742	999	904	462	658	33
28	145	873	421	849	593	383	446	724	8.023	913	445	640	32
29	169	881	405	830	617	392	429	706		922	428	622	31
30	55194	0.07889	83389	0.25811	56641	0.08401	82413	0.24687	58070	0.08931	81412	0.23605	30
31	218	898	373	792	665	409	396	669	094	940	395	587	29
32	242	906	356	773	689	418	380	650		949	378	569	28
33	266	914	340	754	713	427	363	632	141	958	361	552	27
35	315	923	308	735	736	435	347	595	198	967	344	534	25
36			83292	0.25697		0.08453	82314		58212	0.08986	81310	5.16	_
37	55339	948	276	678	808	462	297	0.24577 5 5 9	236	995	293	0.23499	24
38	388	056		659		470		541	260	9004	276	463	22
39	412	956 985	244	640	856	479	264	522	283	013	259	463 446	21
10	436	973	228	621	880	488	248	504	307	022	242	428	20
41	460	982	212	602	804	496	231	486	330	031	225	410	19
12	55484	0.07990	83195	0,25583	56928	0.08505	82214	0.24467	58354	0.09040	81208	0.23393	18
13	509	998	179	564	952	514	198	449	378	049	191	375	17
14	533	8007	163	545	976	523	101	431		058	174	358	16
15	557	015	147		57000	531	165	413	425	067	157	340	15
6	581	024	131	507	024	54	147	399	449	076	140	323	14
17	605	032	115	488	047	549	131	376	472	085	123	305	13
8	55630	0.08041	83098	0.25469		0.08558	82115	0.24358		0.09094	81106	0.23288	12
9	654	049	082	451	095	567	098	340	519	104		270	11
1	678	058		432	119	575	082	3 ²² 3 ⁰⁴	543 567	113	072	253	10
2	792 726		005	413	143	584	048	286	590	131	055	235	9
3	750	075	017	394	191	593 602	032	267	614	140	021	200	7
4	-			-						0.09149		0.23183	6
5	55775	0.08092	2985	338	57215	619	1999	231	661	158	80987	165	5
6	799 823	100	969	330	262	628	982	213		168	970	148	4
7	847	117	953	300	286	637	965	195	708	177	953	130	3
8	871	126	936	282	310	646		177	731	186	936	113	2
9	895	134	920	263	334	655	932	159	755	195	919	096	1
1			D. 5				D.				D. 54		M

	-	. 36.			D	. 37.		is did	D	38.		37/200	
M		S. L. R.	N.S.	S. L. R.	N. S.	S. L. R.	N. S.	S.L.R	N. S.	And the second		S. L. R.	M
0	58779		80902	0.23078	60181	0.0976	79864	0.22054	61566	0.10347	78801	10.21066	60
1 2	802	213		061	205	775	846	037	589	357	783	050	59
3	849	223		043		784		903	7	367	764	033	58
4	873	241	11 0	000	11	803		1987	658	386	729	. 001	57
5	896	250	11 0 1	2991	298	813	776	970	681	396		0985	55
6	58920	0.09259	80799	0.22974	50321	0.09822	79758	0.21953	61704	0.10406		0.20969	
7 8	943	269		957	344	832	741	937	726	416	676	953	53
9	967	278	765	939		841	723	920		426	658	937	52
10	990	296		922	11	861		887	795	436	622	921	50
11	037	306	713	888	437	870	671	870	818	456	604	889	49
12	59061	0.09315	80695	0.22870	60460	0.09880		0.21853	61841	0.10466	78586	0.20872	48
13	084	324	679	853	483	889	635	837	864	476	568	856	47
14	108	338	662	836	506	.899		820		486	550	840	46
15	131	343	644	819	529	909		803 787	909	496 505	532 514	824	45
17	178	361	610	784	576	928	565	770	955	515	496	792	44 43
18	59201	0.09370	80593	0.22767	60599	0.09937	79547	0 21754	61978	0.10525	78478	0.20776	42
19	225	380	576	750	622	947	530	737	2001	535	460	760	41
20	248	389	558	732	645	957	512	720	1	545	442	744	40
21	272	398 408	541	715	668	966		704 687	046	555		728	39
23	295 318	417	524	698	714	986	477	671	009	565	4°5 387	696	38
24	59342	0.09426	80489	0.22664	60738	0.09995	79441	0.21654		0,10585		0.20681	37
25	365	435	472	647	761	10005	424	688	138	595	351	665	35
26	389	445	455	630	784	015	406	621	160	605	333	649	34
27	412	454	438	613	807	024	388	605	183	615	11	633	33
28	436	463	403	595 578	830	034	371 353	588	206	625		601	32
30	59482	0.09482	80386	0.22561	60876	0. 10053	79335		62251	0.10646		0.20585	31
31	506	491	368	544	899	063	318	539	274	656	243	569	30
32	529	501	351	527	922	073	300	522	297	666		553	28
33	552	510	334	510	945	082	282	306	320	676	206	537	27
34	576	520	316	493	958	102	264	490	342	686 696	188	522	26
35	599 59622	529	80282	476	61015	0 10112	79229	473	365 62388	0.10706		506	25
36 37	646	0.09538 548	264	0.22459	038	121	211	0.12457	411	716	78152	0.20490 474	24
38	669	557	247	425	061	131	193	424	433	726	116	458	22
39	693	566	230	478	084	141	179	408	456	736	098	442	21
40	716	576	212	391	107	151		391	479	746	079	.427	20
41	739	585	80178	374	130	160	140	375	502	756		411	19
42 43	59763 786	0.09595	160	0.22357	176	0. 10170	79122	0.21358	548	0.10767 777	78043	0.20395	18
44	800	614	143	323	199	190	087	326	570	787	007	364	16
45	832	623	125	306	222	199	069	309	592	* 797	7988	348	15
46	856	632	108	289	245	209	051	293	515	807	970	332	14
47	879	642	091	273	268	219	033	277	638	817	952	316	13
48	59902	0.09651	056			0.10229	79015	0.21261	62660	0.10827	77934	0.20301	12
49	926 949	670	038	239	314	239	980	244	706	838 848	916	269	11
51	972	680	021	205	360	258	962	212	728	858	879	254	
52	995	689	. 003	188	388	268	944	195	751	868	861	238	8
53	50019		79985	171	406	278	926	179	774	878	843	222	7
54	60042	0.09708	79968	0.22154		0. 10288	78908	0.21163	62796	0.10888	77824	0.20207	6
55	065	718	951	138	451	298	891	147	819	899	806	191	5
57	089	727	934	121	474 497	307	873 855	131	864	909	788 769	175	3.
57 58	135	746	899	087	520	327	837	998	887	929	751	144	2
59	158	756	881	070	543	337	819	082	909	940	733	128	1
M			D.	53.			D.	52.			D.	51.	M

	D	. 39.	1	17 (1)	D	40.			D	. 41.			
M	N.S.	S. L. R.	N.S.	IS. L. R	N. S.	S.L.R.	N. S.	S.L.R		S. L.R.	N. S.	S. L. R.	M
0	62932	13.10950	77715	0.20113		0.11575	76004	3.19193	65606	0.12222	11/277	13.18306	60
2	955	960	696	097	302 323	585		178	650	233	452	291	59
3	977	97° 98°c	660	246	346	606	548	148	672	244	433	277	58
4	022	991	641	050	368	617	530	133	694	266	395	248	57
. 5	045	1001	623	035	390	628	511	118	716	277	375	233	55
6	63068	0.11011	77605	0.20019	54412	0.11638	76492	0.19103	65738	0.12288	75356	0.18219	54
7	090	022	586	004	435	649	473	088	759	299	337	204	53
8	113	032	568	19988	457	660	455	073	781	310	318	190	52
9	135	042	550	973	479	670	436	058	803 825	321	299	175	51
10	158	052	530	957	501	681	417	043	847	332	280	161	50
-	180		513	942	524	-	398		65869	343	261	146	49
12	63203	0.11073	77494	0.19926	568	0.11702	76380 361	0.19093	891	365	75241	0.18132	48
13	225	094	476	895	590	713		983	913	376	203	118	47
1.5	248	104	439	880	612	734	342	968	935	387	184	089	46
16	293	114	421	864	635	745	304	953	956	399	165	074	44
17	316	125	402	849	657	756	286	939	978	410	146	060	43
18	63338	0.11135	77384	0.19834	64679	0.11766	76267	0.18924	66000	0.12423	75126	0.18045	42
19	301	145	366	818	701	777	248	909	022	432	107	031	41
20	383	156	347	803	723	788	229	894	044	443	088	017	40
21	408	166	329	787	746	799	210	879	088	454	069	002	39
22	428	1.76	310	772	768	809	192	864	109	465	050	988	38
23	451	187	292	756	790	820	173	0.18834	-	476	030	7974	37
24	63473	0.11197	77273	0.19741	64812	0.11831	76154	820	153	0.12487	75011	0 17959	36
25	496	207	255	726	834 856	842 852	135	805	175	499	4992	945	35
27	518	228	218	695	878	863	097	7.90	197	521	973	931	34
28	563	239	199	680	901	874	0.78	775	218	532	934	902	33
29	585	249	181	664	923	885	059	760	240	543	915	888	31
30	63608	0.11259	77162	0.19649	64945	0.11895	76041	0.18746	66262	0.12554	74896	0.17874	30
31	630	270	144	634	967	906	022	731	284	566	876	859	29
32	653	28c	125	618	989	917	003	716	3,06	577	857	845	28
33	675	291	107	603	5011	928	5984	686	327	588	838	831	27
34	698	301	088	588	033	939	965	672	349	599 610	818	816	26
35	720	312	070	572	055	0.11960	946	0.18657	66393		799	802	25
36	63742	0:11322	77151	0.19557	65077		75927	642	413	633	74780	0.17788	24
37	765	332	033	542 527	099	971	889	628	436	644	741	774	23
39	810	343		511		993		613	458			745	21
40	832	353 364	977	496	166	2004	851	598	480	666		731	20
41	854	374	959	481	188	015	832	485	501	678	683	717	19
42	63877	0.11385	76940	0.19466	65210	0.12025	75813	0.18569	66523	0.12689	74664	0.17703	18
43	899	395	921	450	232	036	794	554	545	700	644	689	17
44	922	406	903	435	254	047	775	539	566	712	625	674	16
45	944	416	884 866	420		058	756	525	610	723	606	660	15.
46	966	427	847	405	320	080	738	495	632	734 745	586	646	14
47	989	437	-68.9	390			75700	0.18481	66653	0.12757		0.17618	13
	64011	0.11448 458	810	0 19375	65342	0.12091	680	466	675	768	74548 528	604	12
49 50	033	469	791	344	386	. 113		451	697	779	509	590	10
51	078	479		329		. 123	642	437	718	791	489	576	
52	100	490	754	314	430	134	623	422	740	802	470	561	9
53	123	501	735	299	452	145	604	408		813	451	547	7
54	64145	0.11511	76717	0.19284	65474	0.12156	75585	0.18393	66783	0.12825	74431	0.17533	6
55	167	522	698	266	496	167	500	373	805	836	412	519	5
55 56	190	532	679	254	518	178	547	364		847	392	505	4
57	212	543	661	238	540	189		349		859	373	491	3
58	234	553 564	642	223	562	200	509	335 320		870 881	353	471	2
59	256	5041	1)	50.	304		D.			001	334	48.	-
M													

	D.	42.	330 . T. 7	197	D.	43.	1			44-	1	CT	
M	ALE BUILDING	S.L.R.	N. S.	S.L.R.	N. S.	S.L.R.	N. S.	S.L.R.	N. S.	S. L. R.	N S.	S.L.R.	M
0	66913	3.12893	74314	0.17449	68200 I	0.13587	73135	0.16622			A STATE OF THE PARTY OF THE PAR	0.15823	60
1	935	904	295	435	221	599	116	608	487	319	914	810	59
2	956	915	276	421	242	611	099	595	508	331	894	797 784	58
3	978	927	256	407	204	623	076	5.81	529	343	873 853	The second second	57
4	999	938	237	393	285	634	056	554	549	355	833	771	55
5	7021	950	217	379	300			0.16541	_	0.14380	71813		
6	67043	0.12961	74198	0.17365	68327	0.13658 670	73016	527	69591	392	792	731	54
78	084	972	178	351	349	682	976	514	633	404	772	718	52
	100 Sept. 1	The second second	159	337 323	370	694	957	. 500	654	417	752	705	51
9	107	995	120	309	412	705	937	487	675	429	732	692	50
11	151	018	100	295	433	717	917	473	696	441	711	679	49
12	67172	0.13030	74080	0.17281	68455	0.13729	72897	0.16460	69717	0,14453	71691	0.15666	48
13	194	041	061	267	476	741	877	446	737	466	671	653	47
14	215	053	041	253	497	753	857	433	758	478	.650	640	4
15	237	064	022	239	518	765	837	419	779	490	630	627	45
16	258	076		225	539	777	817	406		503	610	615	4
17	280	087	3983	212	561	789	797	392	821	515	590	602	4
18	67301	0.13098	73963	0.17198	68582	0.13800	72777	0.16379	69842	0.14527	71569	0.15589	4
19	323	-110	944	184	603	812	757	366	862	540	549	576	4
20	344	121	The second	170	624	824	737	352		552	529	563	4
21	366	133	11 00-	156		836 848	717	339	904	564	488	550	3
22	387	145		142	The second second	860	697	312	946	589	468	537	3
23	409	156	1					0.16299	11	0.14601			3
24	67430	3.13168		0.17115	68709	0.13872 884	72657	285		614	71447	0.15511	
25	452	179	0	087	730	896	617	272	11	626	466	485	3
26	473	191		073	11 / 3	908	597	259	11.	639	386	472	
27	495	214		059		920	577	245		651	366	460	1 3
29	538	329		045	814	932	557	232		663	345	447	13
-	- 7	The second line	District Co.	0.17032	68835	0.13944	72537	0.16219	70091	0.14676	71325	0.15434	3
30	67559	10.13237		018		956	517	205		688	305	421	2
32	COLUMN TO SERVICE SERV	260		004		968	497	192	132	701	284	408	2
33	623	272	11	6990		980	477	179		713	264	395	2
34	645	28:	649	977	920	992	457	166	174	726		382	
35	666	29		963		4004	437	152	195	738	223	379	2
36	167638	0.13300	73610	10.16949		0.14016	72417	0.16139		0.14750	71203	0.15377	2
37		318		935	983	028	397	1.26		763	182	344	2
38		330	570	922	9004	040		113	257	775	162	331	2
39		341	551	908	025	052		099		800		318	2
40		35		894		064	337	073		813		306	
41	795	30				076	317	0.16060		0.14825		293	
42	67816	0.1337	73491	0.16867		0.14088	72297	0.10300		838	-059	0.15280	
43	837	381		839	109	100	277	033		850	039	255	
44				826	150	124	236	020		863	019	242	4 0000
45	the manufacture of	42		812		136	216	007		875		229	
47	923	43		798		149	196	5994	443	. 888		216	
48		0.1344		0.1678		0.14161	72176		70463	0.14900		0.15204	
49		45	353	77		173	150	967	484	913	937	191	
50	987	479		758	256	185	136	954	505	926	916	178	3 1
51	8008	48	314	744	277	197	116	941	525	938	896	169	
52	929	49	294	739		209		928		951		153	
52	051	50		717		221	075			963		140	
54	THE RESERVE TO BE A SECOND	0.1351	73254	0.1670	69340	0 14234		0.1590		0 14976	70834	0.1512	
59	093	52	234	686		246		808		988			
56		549				268	41		628	5001			
57	136	55		661		270				014			
58	157	56,		649	424	294	11 01 1						
59	1 179	57	155		1 443	7	, 954		390	1 035	711		
		THE RESERVE OF THE PARTY OF THE	D.		The state of the s		D.	46.		-		. 45.	-

LOGARITHMIC SOLAR TABLES

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RISING,

For SIX HOURS,

To EVERY MINUTE and HALF MINUTE.

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M.	S.	H.E.T.	M. T.	R.	H.	O. M.	S.	H.E.T.	M. T.	R.
•	30	2.66121	2.63982	¥ \$27654 \$ 27860	11	30	30	0.87717	4.42386	2.94650
1 1 2	30	18409	3.11694	o. 330y9 58066		31	30	6324	3779	7454 8820
. 2	30	1.96225	33878 41796	77448		32	30	4976	4459 5127 5786	3.00164
3	30	1.81613	3.48490	1. 06673		33	30	0.83669	4.46434	3.02792
4 4	30	75814 0700 66125	54289 9403	28502 37653		34	30	3030 2401 1780	7073 7702	4077 5342
5 5	30	1986	63978 8117 71895	45931 53488		35 35 36	30	1169	8323 8934	6590 7819 9032
6	30	1.54733	3.75370	1. 60440	4	36	30	0.79973	9536	3.10227
7 7 8	30	48520	8588 81583	6877 72869		37	30	9387	0716	2570
8	30	5718 3086	4385	8474 83739	- 0	38	30	8239 7677	1864	3718 4850
9	30	1.38258	9498 3.91845	1. 93399		39	30	0.76574	2981 4•53529	3.17072
10	30	3915 1896	4071 6188 8207	7854 2. 02091 6131	1	40	30	6033 5499 4972	4604	9238
11 11 12	30	29967	4.00136	9991		41 41 42	30	4451 3937	5131 5652 6166	1351
12	30	1.26349,	4.03754	2. 17223 20638		42 43	30	0.73429	4.56674	3.23414
13	30	3010	7093 8617	3915 7073		43	30	2430 1940	7177 7673 8163	5428 6418
14	30	19910	10193	30120	10 /	44	30	1455	8648	7396 8363
15	30	1.17018	4.13085	2. 35910		45	30	0.70503	4.59600	3.29320
16	30	4397 3013	5796 7090	41338		46	30	69571	0532	1202
17	30	1757 0536	8346 9567	6447 8993		47 48	30	8660 8212	1443	3044
18	30	1.09348	4,20755	2. 51271 3586		48	30	7330	4.62334	3·34847 5734
19	30	7067 5970	3036 4133	5841 8039		49	30	6806	3207 3637	6613
20	30	4901 3857	5202 6246	60182		50	30	6041. 5620	4062	9195
21	30	1.02838	4.27265	2. 64316		51 52	30	Q.65204 4791	4.64899	3.40039
22	30	0.99918	9 ² 33 30185	8262 70169		52	30	4383	5720	1702 2522
23	30	8988 8077	2026	2036		53	30	3578	6525	3334
24 25	30	0.97184	4.32919 3793	2. 75652 74°5		54.	30	0.62789	4.67314	3·44935 5724
25 25 26	30	5454 4614	4649 5489	80809		55	30	1632	8089 8471	6507 7282
26	30	3791	7121	4083		56	30	0879	8849 9224	8050
27 27 28	30	0.92189	4·37914 8692	2. 85675 7238		57	30	0.60508	4.69595	3.49566 50314
28	30	89894	9457	8773 90282		58	30	59775	70328 0686	1791
30	30	9156	1673	1765 3223		59	30	9056	1403	2520 3243

M	S.	H.E.T.	M. T.	R.	1. 1.	M.	S.	HET.	M. T.	Ri
.00	30	0.58348	4.71755	3.53959		30	30	0.41488	4.88615	3.88625
9705	THE ST	7999	2104	4670		31	172	261	842	9997
1	30	653	450	5375		31	30	036	9067	557
2	-	310	793	0074		32		0812	291	90034
	30	6970	3133	767		32	30	590 368	513	498
3.		633	470	7455		33	-		735	900
3	30	0.56298	4.73805	3.58137		33	30	0.41049	4.89954	3.91420
4		5966	4137	814		34	- 3	39939	90173	876
4	39	637	466	9486		34	30	7-13	390	2331
5 5 6	-	311	792	60152		35	-	497	606	782
- 3	30	4987	5116	813	-	35	30	282	821	3232
6		666	437	1469		36	1	069	1034	679
	30	9.54347	4.75756	3.62120		36	30	0.38856	4.91247	3.94123
7 7 8	13	931	6072	766		37	1	646	457	566
17	30	3718	385			37	30	436	667	5005
. 0	100	406	697	4043		38	100	227	876	443
8	30	097	7005	675		38	30	020	2083	878
9		2791	312	5302		39		7813	290	6311
9	30	0.52488	4.77615	3.65924		39	30	0.37609	4.92494	3.96742
10	12 3 40	186	917	9542		40	- 35	405	698	7170
.10 .	30	1886	8217	7156		40	30	202	901	597
.11.	TEST SA	589	514	756		41	11 11 11	001	3102	8021
11	30	294	809	8369		41	30	6800	303	443
1.2	115	002	9101	969		42	1	602	501	862
12	30	0.50711	4.79392	3.69566		42	30	0.36404	4.93699	3.99280
13		423	680	70158	111	43	7	206	897	696
13	30	137	966	745		43	30	011	4092	4.00109
14	1	49852	80251	1329		44		5816	287	521
14	30	570	533	909		:44	30	622	481	930
15		290	813	2485		45	33	430	674	1337
15	30	0.49012	4.21001	3.73957			30	0.35238	4.94865	4.01743
16	20	8736	367	625		45	30	047	5056	
16	30	462	641			46	30	4858	245	2146
17	30	189	914	750		47	,	669	434	547
17	30	7919	2184	5397		47.	30	482	621	947
18	3	650	453	860		48	-	296	807	3344
18		0.47883	4.82720			10	20		-	740
	30		984			48	30	0.34110	4.95993	4.04134
19	20	6856		955		49	30	3925	6178	526
19	30		3247	7498		49	30	742	361	916
20	20	595		The second second		50	20	559	5.44	5304
21	30	335	4026	573		50	30	378	725	690
21			4020			51	-	197		6074
	30	0.45822	4.84281	3.79634		51	30	0 33017	4.97085	4.06457
22	100	567	536	80159		52	180	2839		838
22	30	315	788			52	30	661	442	7217
23		064		1201		53	100	485		595
23	30	4815	288	717		53	30	309		
24		567	536	2230		54	-	134	969	8344
24	30	e.44321	4.85782	3.82739		54	30	0.31960	4 98143	4 08716
25	3 118	077	6026			55	1 1 3	787	316	9087
25	30	3834	269			55 56 56	30	614		
26	108	593	510			56	1 3	443	660	823
26	.30	353	750	748		50	30	272		
27	1 325	114				57	1 1 30	103		
27	30	0 42877	4.87226	3.85734		57	30	0.30934	4.99169	
28	1.860	643	460	6223		58	113	766	337	
28	30	409	694			58	30	599		
29)	1000	:176	927	7192		59	1. 330	43	670	992
29	30	1945	8158	672	11	59	30	268	839	
:39	120	716	387	8150	11	60	1 34	10	5 00 po	
		THE RESERVE TO SERVE								

M	8.	H.E.T.	M. T.	R.	н. и.	M.	S.	H.E.T.	M. T.	R.
0	30	0.29939	5.00164	4.13055		30	30	0.21432	5.08671	4.31801
1		776	327	406		31	20	309	794 916	356
1	30	614	489	706		31	30	066	9037	631
2		453	810	4104		32	30	0945	158	906
2	30	293	970	791		33	3	824	279	3180
3	-	133					30	0.20704	5.09399	4.33453
3	30	0.28974	5.01129	4.15140		33	30	585	518	724
4		659		824		34	30	466	637	995
4	30	502	444	6113		35	145	348	755	4265
5 5 6	30	349	757	501		35	30	230	873	534
6	30	191	912	838		36	J. K	113	990	802
6		0,28037	5.02066	4.17173		36	30	0.19996	5.10107	4.35069
	30	7884	219	507		37		880	223	335
7	20	731	372	839		37	30	764	339	601
7 8	30	579	524	8171		38		649	454	865
8	30	428	675	500		38	30	534	569	6128
9	30	277	826	828		39		420	683	391
	-20	0.27127	5.02976	4.19156		39	30	0.19306	5.10797	4.36652
9	30	6978	3125	482		40		193	910	913
10	30	830	275	608		40	30	081	1022	7173
11	3	682	421	20129	111	41		8968	135	432
11	30	535	568	451		41	30	857	246	690
12		389	714	771		42	S142	746	357	948
12	30	0.26244	5.03859	4.21091		42	30	0.18635	5.11468	4.38204
13	30	099	4004	409	1	43		525	578	459
13	30	5955	148	725		43.	30	415	668	714
14	30	811	292	2041		44	1111	306	797	968
14	30	668	435	355		44	30	197	906	9221
15		526	577	668		45	XIII.	089	2014	473.
15	30	0.25385	5.04718	4.22980		45	30	0.17981	5.12122	4.39725
16.	30	244	859	3290		46	100	874	229	975
16	30	104	999	599		46	30	767	336	40225
17		4964	5139	907		47		660	443	474
17	30	825	278	4214		47	30	554	549	722
18	Halles i	687	416	520		48	1	449	654	969
18	30	0,24550	5.05553	4.24825		48	30	0.17344	5.12759	4.41215
19	3 1983	413	690	5128		49	111	239	864	461
19	30	276	827	430		49	30	135	968	706
20		141	962	731	111	50	A Sec.	023	3071	950
20	30	006	6097	6031		50	30	820	175	2193
21		3871	232	330					277	435
21	30	0.23738	5.06365	4.26628		51 52	30	0.16724	5.13379	4.42677
22	1336	605	498	924		52	1153	622	481	918
22	30	472	031	7220		52	30	520	583 684	3158
23	· ·	340	763	514		53		419	784	398 636
23	30	209	894	807		53	30	219	884	874
24		078	7025	8099			-			
24	30	0.22948	5.07155	4.28391		54	30	0.16119	5:13984	4.44111
25	1884	819	284	681		- 55	HES.	020	4083	348
25	30	690	413	969		55	30	5921 823	280	4588 818
20		561	542	9257		56	20	725	378	5052
26	30	433	670	544		57	30	628	47.5	286
27		306	797	830		-57				1 45530
27	30	0.22180	5.07923	4.30115		57 58	30	0.15530	5.14573	4.45518
28		1928	8049	398	1	58	20	434	765	750
28	30	1928	175	684			30	338	861	6212
29	30	803 679	300 424	1963	111	59 59	30	242 146	975	442
29										

MI	S. 1	H.E.T.	м. т.	R. H	. III. M.	S. 1	H.E.T.	M. T.	R.
===	=			-	1 =	=			===
0	30	0.14957	5.15146	4.46899	30	30	0.09981	5.20122	4.59436
1	40	863	230	7127	31		909	194	627 818
1	30	676	334 427	354 580	31	30	837	the second second second	60008
2 2	30	583.	520	806	32 32	30	765	338	198
1 - 10 30	3	490	613	8031	33	30	623	480	387
3 4	30	0.14398	5.15705	4.48255	33	30			4.60576
3	30	307	706	479	34	30	0.09552	5.20551	764
7	30	215	796 888	701	34	30	412	691	952
5 5 6		124	979	924	35		343	760	1139
5	30	034	6069	9145	35	39	273	830	326
6		3944	159	366	36		204	899	512
6	39	0.13854	5.16249	4.49586	36	30	0.09136	5.20967	4.61698
		765	338	806	37		067	1036	883
7 7 8 8	30	676	427	50025	37	30	8999	104	2068
8		5.87	516	243	38	1	931	172	252
	30	399	604	461	38	30	864	239	436
9		411	692	677	39		797	306	619
9	30	0.13324	5.16779	4.50894	39	30	0.08730	5.21373	4.62802
10	1	237	866	1109	40		664	439	984
10	30	150	953	324	40	30	597	506	3166
11		064	7039	539	41		531.	572	347
- 11	30	2978	125	753	41	30	466	637	528
12		893	210	966	42		401	702	708
12	30	0.12807	5.17297	4 52178	42	30	0.08336	5.21767	4.63888
1.3	1	723	380	390	43		271	832	4068
13	30	638	465.	601	43	30	207	896	246
14		554	549	812	44	00 36	143	960	425
14	30	471	632	3022	1 44	30	079	2024	603
15		387	716	231	45	275	015	088	780
15	30	0.12305	5.17798	4.53440	45	30	0.07952	5.22151	4.64957
16	NAME OF	222	881	648	46		889	214	5134
16	30	140	963	856	40	30	827	276	310
17		058		4063	47	TO A ST	865.	338	486
17	30	1977	126	269	47	30	703	400	661
	-	895		475	48		641	462	836
18	30	0.11815		4.54680	48	30	0.07579	5.22524	4.66010
19		734	369		1 49	17 Es.	518	585	184
19	30	654	449	5089	1 49	30	458	645	357
20	30	575 495		293 496	50		397	706 766	530
21	1 30	416		698	50	30	337	826	702
21	30				51		277		874
22	30	0.11338	844	4.55900	51	30	0.07217	5.22886	4.67046
22	30	181	922	301	52	100	099	945	217
23	1	104			52 53	30	040	3004	338
23	30	027			53	30	6982	121	728
24	10.3	0950	153	900	54	30	923	180	897
24	30	0.10873	5.19230		54		0.06865	-	4.68066
25	1	797	306	296	55	30	808	5.23238	
25	30	721	382	494	1 1 55	30	751	352	235 473
25 26 26	1	646	457	690	56	30	693	410	571
26	30	570	533	886	56	30	637	466	738
27		495	608		57		580	523	905
27	30	0.10421	5.19682	4.58277	57	30	0.00524		4.69071
28		347	956	471	58	3	468	5 23579	237
28	30	272		665	58	30	412	691	403
29		199	904		59	238	357	746	568
30	30	126	977	9052	11 59	30	302	801	733
30	1	053	20050	244	60		247	856	897

M	1 S.	H.E.T.	м. т.	R.	H. IV	. M.	S.	H.E.T.	M. T.	R.
0	30	0.06192	5. 23911	4.70061		30	30	0.03399	3.26704	4.79192
1		138	965	224		31	20	360	743	334
1	30	084	4019	387		31	30	283	820	475 615
2		030	073	550		32	30	A Marine Company	858	
3	30	5997 924	179.	874		33	30	245	896	756 896
	-			-			30	-	5.26933	4.80035
3.	30	0.05871	5.24232	4.71030		33 34	30	132	971	I
4 4	1 00	766	337	357		34	30	095	7008	314
	30	714	389	518		35		058	045	455
5 5 6	30	662	441	678		35	30	021	082	491
6	1	610	493	837		36	0	2985	118	729
6	39	0.05559	5.24544	4.71996		36	30	0 02949	5.27154	4.80866
	34	508	595	2155		37	100	913	190	1004
7 7 8	30	457	646	313		37	30	877	226	141
		406	697	471		38	200	841	262	277
8	30	356	747	628		38	30	806	297	414
9		306	797.	785		39		77.1	332	550
9	30	0.05257	5.24846	4.72942		39	30	0.02736	5.27367	4.81686
10		207	896	3098	11	40	811.4	701	402	821
10	30	158	954	254		40	30	667	43 6	956
11		109	994	410		41		633	470	2091
11	30	060	5043	565		41	30	599	504	226
12		012	091	720		42		565	538	360
12	30	0.04964	5.25139	4.73874	1 4 3	42	30	0.02532	5.27571	4.82494
13	7	916	187	4028		43		499	604	628
13	30	868	235	182		43	30	466	637	761
14		821	282	335		44		433	670	894
14	30	774	329	488		44	30	400	703	3025
15		727	376	641	111	45		368	735	159
15	30	0.04580	5.25423	4.74793		45	30	0.02336	5.27767	4.83291
16		588	469	945		46		304	799 830	423
	30		515	5096		47	30	273	852	554 685
17	30	542 496	607	398	98 6 8 6	47	30	210	893	816
18	30	451	652	549		48	30	179	924	947
18		0.04406	5.25697	4.75699		48	30	0.02149	5.27954	4.84077
19	30	361	742	848		49	30	118	985	207
. 19	30	317	786	997		49	30	088	8015	337
20	3	272	831	6146		50	3	058	045	466
20	30	228	875	295		50	30	028	075	595
21	2.19	185	918	443		51		1999	104	724
21	30	0.04141	5.25962	4.76591		51	30	0.01969	5.28134	4 84852
22		098	6005	738		52		940	163	981
. 22	30	055	048	885		52	30	912	191	5108
23	0.5	012	091	7032		53		883	220	236
23	30	3969	134	179		53	30	854	249	303
24		927	176	325		54		826	277	490
24	30	0.03885	5.25218	4.77470		54	30	2.01798	5.28305	4.85617
25	2013	843	260	616		55 55 56	5.3 33	771	332	744
25	30	802	301	761		55	30	743	360	870
25		760	343	936		50	3 H AS	716	387	996
26	30	719 678	384	8050		56	30	689	414	6121
27	-		425	194					441	246
27	30	0.03638	5.26465	4.78338		57 58	.30	0.01635	5.28468	4.86372
28	91111	597	506	481		58		609	494	496
23	30	557	546	624 767		58	30	583	520	621
29		478	586 625	908		59 59 60	30	557	546 572	745 869
30	39	438	665	9051	11,	60	30	531	597	992
201	324 199	1 4301		2.1.		E SERVICES	100	3.0	371	37

M	S.	H.E.T.	М. Т.	R.	H. V.	M.	S.	H.E.T.	M. T.	R.
0	30	0.01 480	5.28623	4.87116	111	30	30	0.00361	15-29742	4.94034
1		455	648	232	111	31	11.77	349	754	141
1	30	430	673	369		31	30	337	766	249
2		406	697	484		32		325	778	356
2	30	381	722	606		32	30	313	790	463
_3		357	746	728	111	33		302	801	570
3	30	0.01333	5.28770	4.87850		33	30	0.00291	5.29812	4.94676
4		310	793	971	111	34		280	823	782
4	30	286	817	8093		34	30	269	834	888
5	-	263	840	213	1111	35		259	844	994
5 5 6	30	240	863 886	334		35 36	30	249	854 864	5100
	-	217		454			-	219		295
6	39	0.01194	5.28909	4.88574		36	30	0.00229	5.29874	4.95310
7 7 8		172	931	694	111	37		219	884	415.
7	30	150	953	814		37 38	30	200	893	520
8	30	106	975	933		38	30	191	903	624 728
9	30	084	997	171	111	39	30	183.	920	83.2
		0.01063		4 89289			-20	-		
9	30	0.01003	5.29040	407		39 40	30	0.00174	5.29929	5.95936
10	39	021	082	\$ 525		40	30	157	937	6040
11	34	000	103	643		41	30	149	946	143
11	30	0980	123	760		41	30	142	961	349
12		960	143	877		42		134	969	451
12	30	0.00940	5.29163	4.89994		42	30	0.00127	5.29976	4 96554
13	30	920	183	90111		43	30	120	983	656
13	30	900	203	227	110	43	30	Y 113	990	758.
14	3	881	222	343		44	3	106	997	860
14	30	862	241	459		44	30	099	30004	961
15		843	260	575		45	1	093	010	7062
	30	0.00824	5.29279	4.90690		45	30	0.00087	5.30016	4.97163
15 16 16		805	298	805		46		081	022	264
16	30	787	316	920		46	30	075	028	365
17		769		1034		47	0.00	070	033	465
17	30	751	352	149		47	30	065	038	565
		733	370	263		48		060	043	665
18	30	0.00716	5.29387	4.91377	111	48	30	0.00055	5-30048	4.97915
19		699	404	490		49	015	050	053	865
19	30	682	421	603		49	30	046	058	964
20		665	428	716		50		041	062	8063
20	30	648	445			50	30	037	066	162
21		632	471	942		51	-	033	070	261
21	30	0.00616	5. 29487	4.92054		51	30	0.00030	5.30073	4 98359
22	20	600	503	166		52		026	077	457
22	30	584	519			52	30	023	080	555
23	30		535	390		53	1 00	017	083	653
24	3-	553	565	612		53	30	015	088	751
	70			-		54			-	849
24	30	0.00523	5.29580	4.92723	111	54	30	0:00013	5 30090	4.98945
25	30		595 6c9	833		55		008	092	9042
25	30	494	623	3054		55	30	007	094	139
26	30	466	637	164		56	30	005	098	235
27		452	651	273		57_	3-	004	099	332 428
27	30	0.00438	5.29665	4.93383			20	0.00003		
28	3	425	678	498		57 58	30	0.00303	5 30100	4 99524
28	30	412	691	6or	1	58	30	100	102	715
29			704	709		59		000	103	810
29	30	399 386	717	817		59	30	000	103	905
30	E BAR	373	730		111	59		000		5.00000

484

EQUATION of TIME.

	1-1-1-					Tarana T									1-	111			-1	100 3				1		
86	Ja	in.	Fe		Ma		Ap			lay		une		uly		lug.		ept.	1	a.	No	ov.	_	ec.		
P	M.	S.	M.	S.	M.	S.	M.		M	. S.	M	. S.	M	L.S.	M	. S.	M		$ \mathbf{M} $. S	M.	S.	M.	S.		
1	14	14	114	15	12	47	3	58	3	14	2	56	12	56	5	38	0	18		16	15	59	10	20		
2	4	42		22		35	3	40	3	22		48	3	7	5	34	0	36	10	34	16	ī	9	56		
		9	14	28	12	22	3	22	3	30	2	39	3	19	5	30	0	55	10	52	16	0	9	32		
3	5	36	14	34	12	8	3 .	3,	3	37	2	29	3	30	5	26	1	14	11	10	15	59	9	8		
5	6		14	38	11	54	25	45	3	43	2	19	3	41	5	20	I	34	II	28	15	57	8	43		
5	6	30	14	42	11	40			3	43	atch too flow	9	3	51	5	14		53	II		15	54	8	17		
7	6	57	14	45		24	23	Q!	3	-53	15	59	4	.0	5	8		12		2	15	51	7.	. 51		
7 8	7	23	14	47	II	9	1-5	51 34	3	57	I O	48	14	8	5	2		32			15	47	70	25		
9	7	48	14		10	54 38	a ta	34	4	1	14	37	4		4	52	2	52		33	15	41	6	59		
10	8	12		49		38	Watch	17	4	4		25	4	22	4	46		13	12	49		35	65	30		
11	8	37	14	49	10	21	1	1	4	7	13	14	4	29	4	37	3	33		4	15	29	645	3		
12	9	2	14	48					4		I	2	4		4.	28	3	53	13	18	15	21	5 4	35		
13	نے و		144	40	9=		0	28	4 3	11	0	50	fait.	53	44	18	How 4	14	135	32	15 8	13	5≥			
14	900	48	14 001	44	Watch too fa	30	0	12	14	12		-3/	5 oot	-0	too faff.	8	42	34	13	46	15 w 51		4	38		
15	100	10		41	92	13	0	18	100	13		25	atch too	7	35	57	4.8	55	138	59	148	53	4	9		
16	100	31	14:0	37	85	55			1=	12	0	13	5-5	13	atch 8	46	5 =	15	14	11	0	41	3	40		
17	10 5	50	74tch 7	32	8 4	37	0	33 ¹ 4	Vatch	11	0	0		18	3 #	34 21 8	5 2	36	14P	23	142	29	3	10		
18	113	9	148	27		19	0 .	48.4	13			13	5≥	24	35	21	55	50	143	34	143	17	2	40		
19	11	271	14	21	8	1		24		11	0	26	5	29	3	8	0	17	14	44	14	3	2	10		
20	11	45.	14	15	7		too flow	16 4		6	0		5	33	-	301		301			13	49	I	40		
100	12	2		7	7	25	10	28 4		3	faff.		5	36	2	42			15	4	13	34	I	11		
22			13	59	7	0	1 = 4	114		0	5 fe	4		39		27			5	13		17	0	41		
23	12	30	13	50	6	47	tch.	54 3		16	1 0	-	5	42	4	13			15		13	0	0	11		
24	2	47		41	6	28	Watch	63		51	atch too			42		58	7	59			12	43		19		
251	3			31	6	10	2> 1	16 3			ato		5	45		42	3	19		34	12	24		49		
	3		**	21	5			27/3		40	13		5	46		26 8				40		5		19		
		28	~	10	5	32 2		8 3		34	4			46		1	100	Ol	_	45		45	19	49		
	3		2	59	5	142		8 3		28 1		20'		45		52 9			5	50 1	I	25	0			
	3	48		-1	4	5512		73	MON 19	21 2		32		44 0		35 9			5	53 1		4	2	47		
3011	3	58		1	4	30/3	•	63		13 2	•	14 5			_	179	-	57	2	-0			0			
3111	4	71		-	4	171		13		5		15		4010		1,		1	5	581		1	3	45		

from thence too flow till the 14th day of April; from thence too flow till the 17th of June.

This Equation of Time is caused by an inequality of the Sun's motion from East to West, according to the succession of sines; for the swifter the Sun is in his annual motion from West to East, the sower he must be in his diurnal motion from East to West.

Watch too fast till the 31st of August; from thence too store till the 23d of December.

A TABLE of SIRIUS,

The GREAT DOG STAR,

PASSING THE

MERIDIAN of GREENWICH.

					_				_						-	34	-	4.	10	-	-	7	_	-
3	Ja	in.	Fe	b.	Ma	rch	Ap	ril	M	ay	Ju	ine		aly	A	ug.	-	pt.	0	a.		OV	D	
Day	H.	M.	H.	M.	H.	M.	H.	M.	H.	M.	H.	M·	H.	M.	H.	M.	H.	M.	H.	M.	H.	M.	H.	M.
	10A	.11	8	4. 7	61	1.23	1 4A	1.30	2/	1.34	I oA	.26	10	M23		124	61	133	41	142	2	M38	OA	127
2	10	6	8	3	6	20	4	26	2	30	0	22	10	19	8	20	6	30	4	39	2	3+	0	22
3	10	2	8	0	6	16	4	22	2	26	0			15	8	17	6	20	4	35	2	30	0	18
4	9	56	7	50	6	12	4	18	2	22	0	18	10	11	8	13	6	22	4	31	2	26	0	13
5	9	52	7	52	6	9	4	15	2	18	0	10	10	7	8	10	6	19	4	27	2	22	0	9
6	9	49	7	48	6	5	4	11	2	14	0	6	10	3	8	6	6	15	4	24	2	18	0	. 4
7 8	9	45	7	44	6	2	4	7	2	10	0	. 1	10	0	8	2	6	12	4	20	2	13	OF	OF
8		41	7	40	5	58	4	3	2	6	111	156	9	56	7	59	6	8	4	16	2	8	II	56
9	9	37	7	37	5	54	4	0	2	1	11	53	9	52	7	56	6	4	4	11	2	0	11	51
10	9	33	7	33	5	50	3	56	1	57	11	49	9	48	7	52.	6	0	4	7	I	59	11	47
11	9	28	7	30	5	46	3	52	I	53		44	9	44	7	48	5	75	4	3	I	55	II	42
12	9	24	7	26	5	43	3	48	I	49		40	9	40	7	44	5	53	3	59	I	50	II	38
13	9	16	7	18	5	39	3	44	I	45	10.00	36	9	36	7	41	5	50	3	55	1	46	II	34
14	9	12	7	14	5	35	3	40	r	40	II	32	9	32 28	7	37 33	5	46	3	51 48	1	42	11	29
15		8	7	-	5		3	36	_	-	-	-	-	-	7	_	5	42	3		1	37	-	25
16		71.00	7	10	5	28	3	32 28	1	32 28	11	24	9	25	7	30	5	38	3	43		33	11	16
17	9	4	7	7	5	24	3	24		24	II	16	9	17	7	23	5	3+	3	39	1	29	II	12
	I a	56	7	3	5	18	3	20		20		12	19	13	7	20	5	30	3	34	I	25	11	8
19	10	53		56	5	14	1 3	17	li	-	II	8	9	9	1 4	16	5	23	3	30	I	15	11	3
21	-	50	-	52	5	11	3	13	-		II	4	9	6	7	12		19	-	-	I	II	10	57
22	10	46		48	5	7		9			II	0	9	2	7	8	5	15	3	23 18	ī	71	10	53
2	1 0	42	6	45		4		5			10	56		58	17	4	5	12	3	14	ī		10	47
24	1 0	38	6	41		o		2		o	10	52	8	54	7	0	5	8	3	10	0	58	10	44
		34		37		56		58	0	56	10	48	8	50	6	57	5	4	3	6	0	54	10	40
25	8	30		34	4	52		54	0	51	10	44	8	46	6	53	5	0	3	2	0	50	10	36
27		26	6	31	14	48	2	50	0	47	10	40	8	43	.6	50	4	57	2	58		45	10	31
2	8, 8	22		27	4	44	2	46		43	10	36	8	39	6	46	4	53	2	5+	0	40	10	27
20	8	18			1 4	40	2	42	10	38	10	31	1-8	35	6	43	4	5	2	50	0	35	10	23
30	8	15			4	37	2	38	0	34	10	27	8	32	6	40	4	46	2	45	0	31	10	19
31	8	11	'		1 4	33	1		0	30	1		8	28	6	36		-	2	42			10	15

TABLEE

The GREAT DOG

How many MILES is a DEGREE

In all LATITUDES.

DL	DL M. tenths D			M. t	enths	DL	M.	tenths	IDL	M. t	enths	DL	М.	enths
=	59	99	19	56	73	37	47	92	55	34	41	73	17	54
2	59	96	20	56	38	38	47	38	56	33	53	74	16	≈ 53
3.	59	92	21	56	OI	39	46	62	57	32	68	75	15	52
4	59	98	22	55	63	40	45	95	58	31	79	76	14	51
5	59	77	23	55	23	41	45	- 28	59	30	90	77	13	50
6	59	67	2.4	54	81	42	44	59	60	30	00.	78	12	48
7	59	56	25	54	38	43	43	88	61	29	19	79	II	45
8	59	42	26	53	93	44	43	16	62	28	17	80	10	42
9	59	26	27	53	56	45	42	43	63	27	24	81	9	38
10	59	08	28	52	97	46	41	68	64	26	30	82	8	35
11	58	89	29	52	47	47	40	92	65	25	36	83	7	32
12	58	68	30	51	96	48	40	15	66	24	41	84	6	28.
13	58	46	31	51	43	49	39	36	67	23	45	85	5.	23
14	58	22	32	50	88	150	38	57	68	22	48	86	4	18
15	57	95	33	50	32	51	37	76	69	21	50	87	3	14
16	57	67	34	49	74	52	36	94	70	20	52	88	2	09
17	57	37	35	49	15	53	36	11	71	19	54	89	1	05
1	57	061	136	48	54	54	35	26	72	18	55			

[This BOOK is ENTERED at STATIONERS-HALL.]

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